Documents

# LM2675 SIMPLE SWITCHER ${ }^{\circledR}$ Power Converter High Efficiency 1-A Step-Down Voltage Regulator 

## 1 Features

- Efficiency up to $96 \%$
- Available in 8-Pin SOIC, PDIP, and 16-Pin WSON Package
- Requires only 5 External Components
- 3.3-V, 5-V, 12-V, and Adjustable Output Versions
- Adjustable Version Output Voltage Range: 1.21 V to 37 V
- $\pm 1.5 \%$ Maximum Output Voltage Tolerance Over Line and Load Conditions
- Ensured 1-A Output Load Current
- Wide Input Voltage Range: 8 V to 40 V
- $260-\mathrm{kHz}$ Fixed Frequency Internal Oscillator
- TTL Shutdown Capability, Low-Power Standby Mode
- Thermal Shutdown and Current Limit Protection


## 2 Applications

- Simple High Efficiency (>90\%) Step-Down (Buck) Regulator
- Efficient Preregulator for Linear Regulators
- Positive-to-Negative Converter


## 3 Description

The LM2675 series of regulators are monolithic integrated DC-DC converter circuits built with a LMDMOS process. These regulators provide all the active functions for a step-down (buck) switching regulator, capable of driving a 1-A load current with excellent line and load regulation. These devices are available in fixed output voltages of $3.3 \mathrm{~V}, 5 \mathrm{~V}, 12 \mathrm{~V}$, and an adjustable output version.

Requiring a minimum number of external components, these regulators are simple to use and include patented internal frequency compensation and a fixed frequency oscillator.

The LM2675 series operates at a switching frequency of 260 kHz , thus allowing smaller-sized filter components than what would be needed with lower frequency switching regulators. Because of its very high efficiency ( $>90 \%$ ), the copper traces on the printed-circuit board are the only heat sinking needed.

| Device Information $^{(\mathbf{1})}$ |  |  |
| :--- | :--- | :---: |
| PART NUMBER | PACKAGE | BODY SIZE (NOM) |
| LM2675 | SOIC $(8)$ | $5.00 \mathrm{~mm} \times 6.20 \mathrm{~mm}$ |
|  | PDIP $(8)$ | $10.16 \mathrm{~mm} \times 6.60 \mathrm{~mm}$ |
|  | WSON $(16)$ | $5.00 \mathrm{~mm} \times 5.00 \mathrm{~mm}$ |

(1) For all available packages, see the orderable addendum at the end of the data sheet.

Typical Application


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NOTE: Page numbers for previous revisions may differ from page numbers in the current version.
Changes from Revision E (June 2005) to Revision F Page

- Added ESD Ratings table, Feature Description section, Device Functional Modes, Application and Implementation section, Power Supply Recommendations section, Layout section, Device and Documentation Support section, and Mechanical, Packaging, and Orderable Information section ..... 1
- Deleted all instances of the computer design software LM267X Made Simple (version 6.0) ..... 1


## 5 Description (continued)

A family of standard inductors for use with the LM2675 are available from several different manufacturers. This feature greatly simplifies the design of switch-mode power supplies using these advanced ICs. Also included in the data sheet are selector guides for diodes and capacitors designed to work in switch-mode power supplies.
Other features include $\pm 1.5 \%$-tolerance on output voltage within specified input voltages and output load conditions, and $\pm 10 \%$ on the oscillator frequency. External shutdown is included, featuring typically $50-\mu \mathrm{A}$ standby current. The output switch includes current limiting, as well as thermal shutdown for full protection under fault conditions.

## 6 Pin Configuration and Functions




## 7 Specifications

### 7.1 Absolute Maximum Ratings

over recommended operating junction temperature range of $-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ (unless otherwise noted) ${ }^{(1)(2)}$

|  |  |  | MIN | MAX | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
| Supply voltage |  |  |  | 45 | V |
| ON/OFF pin voltage, $\mathrm{V}_{\text {SH }}$ |  |  | -0.1 | 6 | V |
| Switch voltage to ground |  |  |  | -1 | V |
| Boost pin voltage |  |  |  | $\mathrm{V}_{\mathrm{SW}}+8$ | V |
| Feedback pin voltage, $\mathrm{V}_{\mathrm{FB}}$ |  |  | -0.3 | 14 | V |
| Power dissipation |  |  | Inte | mited |  |
| Lead temperature | D package | Vapor phase (60 s) |  | 215 | ${ }^{\circ} \mathrm{C}$ |
|  |  | Infrared (15 s) |  | 220 |  |
|  | P package (soldering, 10 s ) |  |  | 260 |  |
|  | NHN package |  | See AN-1187 |  |  |
| Maximum junction temperature, $\mathrm{T}_{J}$ |  |  |  | 150 | ${ }^{\circ} \mathrm{C}$ |
| Storage temperature, $\mathrm{T}_{\text {stg }}$ |  |  | -65 | 150 | ${ }^{\circ} \mathrm{C}$ |

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.
(2) If Military/Aerospace specified devices are required, contact the Texas Instruments Sales Office/ Distributors for availability and specifications.

### 7.2 ESD Ratings

| \begin{tabular}{c\|c|c|}
\hline
\end{tabular} |  |  | VALUE |
| :--- | :--- | :---: | :---: |
| $V_{(E S D)}$ | Electrostatic discharge | Human-body model (HBM), per ANSI/ESDA/JEDEC JS-001 ${ }^{(1)(2)}$ | $\pm 2000$ |

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.
(2) The human-body model is a $100-\mathrm{pF}$ capacitor discharged through a $1.5-\mathrm{k} \Omega$ resistor into each pin.

### 7.3 Recommended Operating Conditions

over operating free-air temperature range (unless otherwise noted)

|  | Supply voltage | MIN | MAX |
| :--- | :--- | ---: | ---: |
|  | UNIT |  |  |
| $T_{J}$ | Temperature | 6.5 | 40 |

### 7.4 Thermal Information

| THERMAL METRIC ${ }^{(1)(2)}$ |  | LM2675 |  |  | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SOIC (D) | PDIP (P) | NHN (WSON) |  |
|  |  | 8 PINS | 8 PINS | 16 PINS |  |
| $\mathrm{R}_{\theta \mathrm{JA}}$ | Junction-to-ambient thermal resistance ${ }^{(3)}$ | 105 | 95 | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\text {日JC(top) }}$ | Junction-to-case (top) thermal resistance | - | - | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\theta \mathrm{JB}}$ | Junction-to-board thermal resistance | - | - | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\Psi_{\text {JT }}$ | Junction-to-top characterization parameter | - | - | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\psi_{\text {JB }}$ | Junction-to-board characterization parameter | - | - | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |
| $\mathrm{R}_{\text {日JC(bot) }}$ | Junction-to-case (bottom) thermal resistance | - | - | - | ${ }^{\circ} \mathrm{C} / \mathrm{W}$ |

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report.
(2) Thermal resistances were simulated on 4-layer JEDEC board.
(3) Junction-to-ambient thermal resistance with approximately 1 square inch of printed-circuit board copper surrounding the leads. Additional copper area lowers thermal resistance further. See Application Information in the application note accompanying this data sheet. The value $\mathrm{R}_{\theta \mathrm{JA}}$ for the WSON (NHN) package is specifically dependent on PCB trace area, trace material, and the number of layers and thermal vias. For improved thermal resistance and power dissipation for the WSON package, refer to AN-1187 Leadless Leadframe Package (LLP).

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### 7.5 Electrical Characteristics - 3.3 V

$\mathrm{T}_{J}=25^{\circ} \mathrm{C}$ (unless otherwise noted; see Figure 19) ${ }^{(1)}$

|  | ARAMETER | TEST CONDITIONS |  | $\mathbf{M I N}{ }^{(2)}$ | TYP ${ }^{(3)}$ | MAX ${ }^{(2)}$ | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Vout | Output voltage | $\mathrm{V}_{\mathrm{IN}}=8 \mathrm{~V}$ to $40 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=20 \mathrm{~mA}$ to 1 A | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ | 3.251 | 3.3 | 3.35 | V |
|  |  |  | $\mathrm{T}_{\mathrm{J}}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 3.201 |  | 3.399 |  |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=6.5 \mathrm{~V} \text { to } 40 \mathrm{~V}, \\ & \mathrm{I}_{\text {LOAD }}=20 \mathrm{~mA} \text { to } 500 \mathrm{~mA} \end{aligned}$ | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ | 3.251 | 3.3 | 3.35 |  |
|  |  |  | $\mathrm{T}_{\mathrm{J}}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 3.201 |  | 3.399 |  |
| $\eta$ | Efficiency | $\mathrm{V}_{\text {IN }}=12 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=1 \mathrm{~A}$ |  | 86\% |  |  |  |

(1) External components such as the catch diode, inductor, input and output capacitors, and voltage programming resistors can affect switching regulator performance. When the LM2675 is used as shown in Figure 19 test circuits, system performance is as specified by the system parameters section of Electrical Characteristics.
(2) All limits specified at room temperature and at temperature extremes. All room temperature limits are $100 \%$ production tested. All limits at temperature extremes are specified through correlation using standard Statistical Quality Control (SQC) methods. All limits are used to calculate Average Outgoing Quality Level (AOQL).
(3) Typical numbers are at $25^{\circ} \mathrm{C}$ and represent the most likely norm.

### 7.6 Electrical Characteristics - 5 V

$\mathrm{T}_{J}=25^{\circ} \mathrm{C}$ (unless otherwise noted; see Figure 19) ${ }^{(1)}$

| PARAMETER |  | TEST CONDITIONS |  | MIN ${ }^{(2)}$ | TYP ${ }^{(3)}$ | MAX ${ }^{(2)}$ | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {OUT }}$ | Output voltage | $\mathrm{V}_{\text {IN }}=8 \mathrm{~V}$ to 40 V , $\mathrm{L}_{\text {LOAD }}=20 \mathrm{~mA}$ to 1 A | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ | 4.925 | 5 | 5.075 | V |
|  |  |  | $\mathrm{T}_{J}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 4.85 |  | 5.15 |  |
|  |  | $\begin{aligned} & \mathrm{V}_{\mathrm{IN}}=6.5 \mathrm{~V} \text { to } 40 \mathrm{~V}, \\ & \mathrm{I}_{\mathrm{LOAD}}=20 \mathrm{~mA} \text { to } 500 \mathrm{~mA} \end{aligned}$ | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ | 4.925 | 5 | 5.075 |  |
|  |  |  | $\mathrm{T}_{J}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 4.85 |  | 5.15 |  |
| $\eta$ | Efficiency | $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=1 \mathrm{~A}$ |  | 90\% |  |  |  |

(1) External components such as the catch diode, inductor, input and output capacitors, and voltage programming resistors can affect switching regulator performance. When the LM2675 is used as shown in Figure 19 test circuits, system performance is as specified by the system parameters section of Electrical Characteristics.
(2) All limits specified at room temperature and at temperature extremes. All room temperature limits are $100 \%$ production tested. All limits at temperature extremes are specified through correlation using standard Statistical Quality Control (SQC) methods. All limits are used to calculate Average Outgoing Quality Level (AOQL).
(3) Typical numbers are at $25^{\circ} \mathrm{C}$ and represent the most likely norm.

### 7.7 Electrical Characteristics - 12 V

$\mathrm{T}_{J}=25^{\circ} \mathrm{C}$ (unless otherwise noted; see Figure 19) ${ }^{(1)}$

| PARAMETER |  | TEST CONDITIONS |  | MIN ${ }^{(2)}$ | TYP ${ }^{(3)}$ | MAX ${ }^{(2)}$ | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{V}_{\text {OUT }}$ | Output voltage | $\mathrm{V}_{\mathrm{IN}}=15 \mathrm{~V}$ to $40 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=20 \mathrm{~mA}$ to 1 A | $\mathrm{T}_{J}=25^{\circ} \mathrm{C}$ | 11.82 | 12 | 12.18 | V |
|  |  |  | $\mathrm{T}_{\mathrm{J}}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 11.64 |  | 12.36 |  |
| $\eta$ | Efficiency | $\mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=1 \mathrm{~A}$ |  | 94\% |  |  |  |

(1) External components such as the catch diode, inductor, input and output capacitors, and voltage programming resistors can affect switching regulator performance. When the LM2675 is used as shown in Figure 19 test circuits, system performance is as specified by the system parameters section of Electrical Characteristics.
(2) All limits specified at room temperature and at temperature extremes. All room temperature limits are $100 \%$ production tested. All limits at temperature extremes are specified through correlation using standard Statistical Quality Control (SQC) methods. All limits are used to calculate Average Outgoing Quality Level (AOQL).
(3) Typical numbers are at $25^{\circ} \mathrm{C}$ and represent the most likely norm.

### 7.8 Electrical Characteristics - Adjustable

$\mathrm{T}_{J}=25^{\circ} \mathrm{C}$ (unless otherwise noted; see Figure 19) ${ }^{(1)}$

|  | ARAMETER | TEST CONDITIONS |  | MIN ${ }^{(2)}$ | TYP ${ }^{(3)}$ | MAX ${ }^{(2)}$ | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $V_{\text {FB }}$ | Feedback voltage | $\mathrm{V}_{\mathrm{IN}}=8 \mathrm{~V}$ to 40 V , $\mathrm{I}_{\text {LOAD }}=20 \mathrm{~mA}$ to 1 A , $V_{\text {OUT }}$ programmed for 5 V (see Figure 19) | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ | 1.192 | 1.21 | 1.228 | V |
|  |  |  | $\mathrm{T}_{J}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 1.174 |  | 1.246 |  |
|  |  | $\mathrm{V}_{\mathrm{IN}}=6.5 \mathrm{~V}$ to $40 \mathrm{~V}, \mathrm{I}_{\mathrm{LOAD}}=20 \mathrm{~mA}$ to 500 $\mathrm{mA}, \mathrm{V}_{\text {Out }}$ programmed for 5 V (see Figure 19) | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ | 1.192 | 1.21 | 1.228 |  |
|  |  |  | $\mathrm{T}_{J}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 1.174 |  | 1.246 |  |
| $\eta$ | Efficiency | $\mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}, \mathrm{I}_{\text {LOAD }}=1 \mathrm{~A}$ |  | 90\% |  |  |  |

(1) External components such as the catch diode, inductor, input and output capacitors, and voltage programming resistors can affect switching regulator performance. When the LM2675 is used as shown in Figure 19 test circuits, system performance is as specified by the system parameters section of Electrical Characteristics.
(2) All limits specified at room temperature and at temperature extremes. All room temperature limits are $100 \%$ production tested. All limits at temperature extremes are specified through correlation using standard Statistical Quality Control (SQC) methods. All limits are used to calculate Average Outgoing Quality Level (AOQL).
(3) Typical numbers are at $25^{\circ} \mathrm{C}$ and represent the most likely norm.

### 7.9 Electrical Characteristics - All Output Voltage Versions

$\mathrm{T}_{J}=25^{\circ} \mathrm{C}, \mathrm{V}_{\mathrm{IN}}=12 \mathrm{~V}$ for the $3.3 \mathrm{~V}, 5 \mathrm{~V}$, and adjustable versions, and $\mathrm{V}_{\mathrm{IN}}=24 \mathrm{~V}$ for the 12 V version, and $\mathrm{I}_{\mathrm{LOAD}}=100 \mathrm{~mA}$ (unless otherwise noted)

|  | PARAMETER | TEST CONDITIONS |  | $\mathbf{M I N}{ }^{(1)}$ | TYP ${ }^{(2)}$ | MAX ${ }^{(1)}$ | UNIT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| $\mathrm{I}_{\mathrm{Q}}$ | Quiescent current | $\mathrm{V}_{\text {FEEDBACK }}=8 \mathrm{~V}$ for 3.3 V , 5 V , and adjustable versions |  |  | 2.5 | 3.6 | mA |
|  |  | $\mathrm{V}_{\text {FEEDBACK }}=15 \mathrm{~V}$ for 12 V versions |  |  | 2.5 |  | mA |
| $I_{\text {STBY }}$ | Standby quiescent current | ON/OFF Pin $=0 \mathrm{~V}$ | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  | 50 | 100 |  |
|  |  |  | $\mathrm{T}_{J}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  |  | 150 | $\mu \mathrm{A}$ |
| ICL | Current limit | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  | 1.25 | 1.55 | 2.1 |  |
|  |  | $\mathrm{T}_{J}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | 1.2 |  | 2.2 | A |
| L | Output leakage current | $\mathrm{V}_{\text {SWITCH }}=0 \mathrm{~V}$, ON/OFF Pin $=0 \mathrm{~V}, \mathrm{~V}_{\text {IN }}=40 \mathrm{~V}$ |  |  | 1 | 25 | $\mu \mathrm{A}$ |
|  |  | $\mathrm{V}_{\text {SWITCH }}=-1 \mathrm{~V}$, ON/OFF Pin $=0 \mathrm{~V}$ |  |  | 6 | 15 | mA |
| $\mathrm{R}_{\mathrm{DS}(\mathrm{ON})}$ | Switch on-resistance | $\mathrm{ISWITCH}=1 \mathrm{~A}$ | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  | 0.25 | 0.3 | $\Omega$ |
|  |  |  | $\mathrm{T}_{J}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  |  | 0.5 |  |
| $\mathrm{fo}_{0}$ | Oscillator frequency | Measured at switch pin | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  | 260 |  | kHz |
|  |  |  | $\mathrm{T}_{J}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 225 |  | 275 | Hz |
| D | Minimum duty cycle | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  |  | 95\% |  |  |
|  |  | $\mathrm{T}_{\mathrm{J}}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  |  | 0\% |  |  |
| $\mathrm{I}_{\text {BIAS }}$ | Feedback bias current | $\mathrm{V}_{\text {FEEDBACK }}=1.3 \mathrm{~V}$, adjustable version only |  |  | 85 |  | nA |
| $\mathrm{V}_{\mathrm{S} / \mathrm{D}}$ | ON/ $\overline{\text { OFF }}$ pin voltage | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  |  | 1.4 |  | V |
|  |  | $\mathrm{T}_{\mathrm{J}}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ |  | 0.8 |  | 2 |  |
| $\mathrm{I}_{\text {S/D }}$ | ON/OFF pin current | ON/OFF Pin $=0 \mathrm{~V}$ | $\mathrm{T}_{\mathrm{J}}=25^{\circ} \mathrm{C}$ |  | 20 |  | $\mu \mathrm{A}$ |
|  |  |  | $\mathrm{T}_{J}=-40^{\circ} \mathrm{C}$ to $125^{\circ} \mathrm{C}$ | 7 |  | 37 |  |

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### 7.10 Typical Characteristics



## Typical Characteristics (continued)



Figure 7. Standby Quiescent Current


Figure 9. ON/OFF Pin Current (Sourcing)


JUNCTION TEMPERATURE ( ${ }^{\circ} \mathrm{C}$ )
Figure 11. Feedback Pin Bias Current


Figure 8. ON/OFF Threshold Voltage


Figure 10. Switching Frequency


Figure 12. Peak Switch Current

## Typical Characteristics (continued)



Figure 13. Dropout Voltage, 3.3-V Option


Figure 14. Dropout Voltage, 5-V Option

### 7.11 Typical Characteristics - Fixed Output Voltage Versions

see Figure 19


Figure 15. Continuous Mode Switching Waveforms, Horizontal Time Base: $\mathbf{1} \boldsymbol{\mu s} /$ div


Figure 17. Load Transient Response for Continuous Mode, Horizontal Time Base: $\mathbf{5 0} \boldsymbol{\mu s} / \mathrm{div}$


Figure 16. Discontinuous Mode Switching Waveforms, Horizontal Time Base: $\mathbf{1} \mu \mathrm{s} / \mathrm{div}$


Figure 18. Load Transient Response for Discontinuous Mode, Horizontal Time Base: $200 \mu \mathrm{~s} / \mathrm{div}$

## 8 Detailed Description

### 8.1 Overview

The LM2675 provides all of the active functions required for a step-down (buck) switching regulator. The internal power switch is a DMOS power MOSFET to provide power supply designs with high current capability, up to 1 A, and highly efficient operation. The LM2675 is part of the SIMPLE SWITCHER ${ }^{\circledR}$ family of power converters. A complete design uses a minimum number of external components, which have been predetermined from a variety of manufacturers. Using either this data sheet or Tl's WEBENCH® design tool, a complete switching power supply can be designed quickly. See LM2670 SIMPLE SWITCHER ${ }^{\circledR}$ High Efficiency 3A Step-Down Voltage Regulator with Sync for additional application information.

### 8.2 Functional Block Diagram



### 8.3 Feature Description

### 8.3.1 Adjustable Output Voltage

The voltage regulation loop in the LM2675 regulates output voltage by maintaining the voltage on FB pin $\left(\mathrm{V}_{\mathrm{FB}}\right)$ to be the same as the internal REF voltage ( $\mathrm{V}_{\text {REF }}$ ). A resistor divider pair is needed to program the ratio from output voltage $\mathrm{V}_{\text {OUT }}$ to $\mathrm{V}_{\text {FB }}$. The resistor is connected from the $\mathrm{V}_{\text {OUt }}$ of the LM2674 to ground with the mid-point connecting to the FB pin. The voltage reference system produces a precise voltage reference over temperature. The internal REF voltage is typically 1.21 V . To program the output voltage of the LM2675 to be a certain value $V_{\text {OUT }}$, R1 can be calculated with a selected R2. See Programming Output Voltage for adjustable output voltage typical application. The recommended range for R2 in most application is from $10 \mathrm{k} \Omega$ to $100 \mathrm{k} \Omega$. If the resistor divider is not connected properly, output voltage cannot be regulated because the feedback loop is broken. If the FB pin is shorted to ground, the output voltage is driven close to VIN, because the regulator sees very low voltage on the FB pin and tries to regulate it. The load connected to the output could be damaged under such a condition. Do not short FB pin to ground when the LM2675 is enabled. It is important to route the feedback trace away from the noisy area of the PCB. For more layout recommendations, see Layout.

### 8.4 Device Functional Modes

### 8.4.1 Shutdown Mode

The ON/OFF pin provides electrical ON and OFF control for the LM2674. When the voltage of this pin is lower than 1.4 V , the device is in shutdown mode. The typical standby current in this mode is $20 \mu \mathrm{~A}$.

### 8.4.2 Active Mode

When the voltage of the ON/OFF pin is higher than 1.4 V , the device starts switching and the output voltage rises until it reaches a normal regulation voltage.

## 9 Application and Implementation

## NOTE

Information in the following applications sections is not part of the Tl component specification, and TI does not warrant its accuracy or completeness. Tl's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

### 9.1 Application Information

The LM2675 is a step-down DC-DC regulator. The device is typically used to convert a higher DC voltage to a lower DC voltage with a maximum output current of 1 A . The following design procedure can be used to select components for the LM2675.
When the output voltage is greater than approximately 6 V , and the duty cycle at minimum input voltage is greater than approximately $50 \%$, the designer should exercise caution in selection of the output filter components. When an application designed to these specific operating conditions is subjected to a current limit fault condition, it may be possible to observe a large hysteresis in the current limit. This can affect the output voltage of the device until the load current is reduced sufficiently to allow the current limit protection circuit to reset itself.

Under current limiting conditions, the LM2675 is designed to respond in the following manner:

1. At the moment when the inductor current reaches the current limit threshold, the ON-pulse is immediately terminated. This happens for any application condition.
2. However, the current limit block is also designed to momentarily reduce the duty cycle to below $50 \%$ to avoid subharmonic oscillations, which could cause the inductor to saturate.
3. Thereafter, once the inductor current falls below the current limit threshold, there is a small relaxation time during which the duty cycle progressively rises back above $50 \%$ to the value required to achieve regulation.
If the output capacitance is sufficiently large, it may be possible that as the output tries to recover, the output capacitor charging current is large enough to repeatedly re-trigger the current limit circuit before the output has fully settled. This condition is exacerbated with higher output voltage settings because the energy requirement of the output capacitor varies as the square of the output voltage ( $1 / 2 \mathrm{CV}$ ), thus requiring an increased charging current. A simple test to determine if this condition might exist for a suspect application is to apply a short circuit across the output of the converter, and then remove the shorted output condition. In an application with properly selected external components, the output recovers smoothly. Practical values of external components that have been experimentally found to work well under these specific operating conditions are COUT $=47 \mu \mathrm{~F}$, $\mathrm{L}=22 \mu \mathrm{H}$. It should be noted that even with these components, for a device's current limit of $\mathrm{I}_{\mathrm{CLIM}}$, the maximum load current under which the possibility of the large current limit hysteresis can be minimized is $\mathrm{I}_{\text {Clim }} / 2$. For example, if the input is 24 V and the set output voltage is 18 V , then for a desired maximum current of 1.5 A , the current limit of the chosen switcher must be confirmed to be at least 3 A. Under extreme overcurrent or shortcircuit conditions, the LM2675 employs frequency foldback in addition to the current limit. If the cycle-by-cycle inductor current increases above the current limit threshold (due to short circuit or inductor saturation for example) the switching frequency is automatically reduced to protect the IC. Frequency below 100 kHz is typical for an extreme short-circuit condition.

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### 9.2 Typical Application

### 9.2.1 Fixed Output Voltage Application



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$\mathrm{C}_{\mathrm{IN}}=22-\mu \mathrm{F}, 50-\mathrm{V}$ Tantalum, Sprague 199D Series
$\mathrm{C}_{\text {OUt }}=47-\mu \mathrm{F}, 25-\mathrm{V}$ Tantalum, Sprague 595D Series
D1 = 3.3-A, 50-V Schottky Rectifier, IR 30WQ05F
L1 $=68-\mu \mathrm{H}$ Sumida \#RCR110D-680L
$C_{B}=0.01-\mu F, 50-\mathrm{V}$ Ceramic
Figure 19. Fixed Output Voltage Schematic

### 9.2.1.1 Design Requirements

Table 1 lists the design requirements for the fixed output voltage application.
Table 1. Design Parameters

| PARAMETER | VALUE |
| :---: | :---: |
| Regulated output voltage, $\mathrm{V}_{\text {OUT }}$ | 5 V |
| Maximum input voltage, $\mathrm{V}_{\text {IN }}(\max )$ | 12 V |
| Maximum load current, $\mathrm{I}_{\text {LOAD }}(\max )$ | 1 A |

### 9.2.1.2 Detailed Design Procedure

### 9.2.1.2.1 Inductor Selection (L1)

Select the correct inductor value selection guide from Figure 21, Figure 22, or Figure 23 (output voltages of $3.3 \mathrm{~V}, 5 \mathrm{~V}$, or 12 V respectively). For all other voltages, see Detailed Design Procedure. Use the inductor selection guide for the 5-V version shown in Figure 22.

From the inductor value selection guide, identify the inductance region intersected by the maximum input voltage line and the maximum load current line. Each region is identified by an inductance value and an inductor code (LXX). From the inductor value selection guide shown in Figure 22, the inductance region intersected by the 12-V horizontal line and the 1-A vertical line is $33 \mu \mathrm{H}$, and the inductor code is L23.

Select an appropriate inductor from the four manufacturer's part numbers listed in Table 2. Each manufacturer makes a different style of inductor to allow flexibility in meeting various design requirements. The inductance value required is $33 \mu \mathrm{H}$. From the table in Table 2, go to the L23 line and choose an inductor part number from any of the four manufacturers shown. In most instances, both through hole and surface mount inductors are available.

Table 2. Inductor Manufacturers' Part Numbers

|  | INDUCTANCE ( $\mu \mathrm{H}$ ) | CURRENT <br> (A) | SCHOTT |  | RENCO |  | PULSE ENGINEERING |  | COILCRAFT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | THROUGH HOLE | SURFACE MOUNT | THROUGH HOLE | SURFACE MOUNT | THROUGH HOLE | SURFACE MOUNT | SURFACE MOUNT |
| L4 | 68 | 0.32 | 67143940 | 67144310 | RL-1284-68-43 | RL1500-68 | PE-53804 | PE-53804-S | DO1608-683 |
| L5 | 47 | 0.37 | 67148310 | 67148420 | RL-1284-47-43 | RL1500-47 | PE-53805 | PE-53805-S | DO1608-473 |
| L6 | 33 | 0.44 | 67148320 | 67148430 | RL-1284-33-43 | RL1500-33 | PE-53806 | PE-53806-S | DO1608-333 |
| L7 | 22 | 0.52 | 67148330 | 67148440 | RL-1284-22-43 | RL1500-22 | PE-53807 | PE-53807-S | DO1608-223 |
| L9 | 220 | 0.32 | 67143960 | 67144330 | RL-5470-3 | RL1500-220 | PE-53809 | PE-53809-S | DO3308-224 |
| L10 | 150 | 0.39 | 67143970 | 67144340 | RL-5470-4 | RL1500-150 | PE-53810 | PE-53810-S | DO3308-154 |
| L11 | 100 | 0.48 | 67143980 | 67144350 | RL-5470-5 | RL1500-100 | PE-53811 | PE-53811-S | DO3308-104 |
| L12 | 68 | 0.58 | 67143990 | 67144360 | RL-5470-6 | RL1500-68 | PE-53812 | PE-53812-S | DO3308-683 |
| L13 | 47 | 0.7 | 67144000 | 67144380 | RL-5470-7 | RL1500-47 | PE-53813 | PE-53813-S | DO3308-473 |
| L14 | 33 | 0.83 | 67148340 | 67148450 | RL-1284-33-43 | RL1500-33 | PE-53814 | PE-53814-S | DO3308-333 |
| L15 | 22 | 0.99 | 67148350 | 67148460 | RL-1284-22-43 | RL1500-22 | PE-53815 | PE-53815-S | DO3308-223 |
| L18 | 220 | 0.55 | 67144040 | 67144420 | RL-5471-2 | RL1500-220 | PE-53818 | PE-53818-S | DO3316-224 |
| L19 | 150 | 0.66 | 67144050 | 67144430 | RL-5471-3 | RL1500-150 | PE-53819 | PE-53819-S | DO3316-154 |
| L20 | 100 | 0.82 | 67144060 | 67144440 | RL-5471-4 | RL1500-100 | PE-53820 | PE-53820-S | DO3316-104 |
| L21 | 68 | 0.99 | 67144070 | 67144450 | RL-5471-5 | RL1500-68 | PE-53821 | PE-53821-S | DO3316-683 |
| L22 | 47 | 1.17 | 67144080 | 67144460 | RL-5471-6 | - | PE-53822 | PE-53822-S | DO3316-473 |
| L23 | 33 | 1.4 | 67144090 | 67144470 | RL-5471-7 | - | PE-53823 | PE-53823-S | DO3316-333 |
| L24 | 22 | 1.7 | 67148370 | 67148480 | RL-1283-22-43 | - | PE-53824 | PE-53824-S | DO3316-223 |
| L27 | 220 | 1 | 67144110 | 67144490 | RL-5471-2 | - | PE-53827 | PE-53827-S | DO5022P-224 |
| L28 | 150 | 1.2 | 67144120 | 67144500 | RL-5471-3 | - | PE-53828 | PE-53828-S | DO5022P-154 |
| L29 | 100 | 1.47 | 67144130 | 67144510 | RL-5471-4 | - | PE-53829 | PE-53829-S | DO5022P-104 |
| L30 | 68 | 1.78 | 67144140 | 67144520 | RL-5471-5 | - | PE-53830 | PE-53830-S | DO5022P-683 |

### 9.2.1.2.2 Output Capacitor Selection (Cout)

Select an output capacitor from Table 3. Using the output voltage and the inductance value found in the inductor selection guide, step 1, locate the appropriate capacitor value and voltage rating. The capacitor list contains through-hole electrolytic capacitors from four different capacitor manufacturers and surface mount tantalum capacitors from two different capacitor manufacturers. TI recommends using both the manufacturers and the manufacturer's series that are listed in the table.

Use the $5-\mathrm{V}$ section in Table 3. Choose a capacitor value and voltage rating from the line that contains the inductance value of $33 \mu \mathrm{H}$. The capacitance and voltage rating values corresponding to the $33-\mu \mathrm{H}$ inductor are the surface mount and through hole.
Surface mount:

- 68- $\mu \mathrm{F}, 10-\mathrm{V}$ Sprague 594D series
- 100- $\mu \mathrm{F}, 10-\mathrm{V}$ AVX TPS series

Through hole:

- $68-\mu \mathrm{F}, 10-\mathrm{V}$ Sanyo OS-CON SA series
- $220-\mu \mathrm{F}, 35-\mathrm{V}$ Sanyo MV-GX series
- $220-\mu \mathrm{F}, 35-\mathrm{V}$ Nichicon PL series
- $220-\mu \mathrm{F}, 35-\mathrm{V}$ Panasonic HFQ series

Table 3. Output Capacitor Table

| OUTPUT VOLTAGE (V) | INDUCTANCE ( $\mu \mathrm{H}$ ) | OUTPUT CAPACITOR |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | SURFACE MOUNT |  | THROUGH HOLE |  |  |  |
|  |  | $\begin{aligned} & \text { SPRAGUE } \\ & \text { 594D SERIES } \\ & (\mu F / V) \end{aligned}$ | AVX TPS SERIES ( $\mu \mathrm{F} / \mathrm{V}$ ) | SANYO OS-CON SA SERIES ( $\mu \mathrm{F} / \mathrm{V}$ ) | SANYO MV-GX SERIES ( $\mu \mathrm{F} / \mathrm{V}$ ) | NICHICON PL SERIES ( $\mu \mathrm{F} / \mathrm{V}$ ) | PANASONIC HFQ SERIES ( $\mu \mathrm{F} / \mathrm{V}$ ) |
| 3.3 | 22 | 120/6.3 | 100/10 | 100/10 | 330/35 | 330/35 | 330/35 |
|  | 33 | 120/6.3 | 100/10 | 68/10 | 220/35 | 220/35 | 220/35 |
|  | 47 | 68/10 | 100/10 | 68/10 | 150/35 | 150/35 | 150/35 |
|  | 68 | 120/6.3 | 100/10 | 100/10 | 120/35 | 120/35 | 120/35 |
|  | 100 | 120/6.3 | 100/10 | 100/10 | 120/35 | 120/35 | 120/35 |
|  | 150 | 120/6.3 | 100/10 | 100/10 | 120/35 | 120/35 | 120/35 |
| 5 | 22 | 100/16 | 100/10 | 100/10 | 330/35 | 330/35 | 330/35 |
|  | 33 | 68/10 | 10010 | 68/10 | 220/35 | 220/35 | 220/35 |
|  | 47 | 68/10 | 100/10 | 68/10 | 150/35 | 150/35 | 150/35 |
|  | 68 | 100/16 | 100/10 | 100/10 | 120/35 | 120/35 | 120/35 |
|  | 100 | 100/16 | 100/10 | 100/10 | 120/35 | 120/35 | 120/35 |
|  | 150 | 100/16 | 100/10 | 100/10 | 120/35 | 120/35 | 120/35 |
| 12 | 22 | 120/20 | (2x) 68/20 | 68/20 | 330/35 | 330/35 | 330/35 |
|  | 33 | 68/25 | 68/20 | 68/20 | 220/35 | 220/35 | 220/35 |
|  | 47 | 47/20 | 68/20 | 47/20 | 150/35 | 150/35 | 150/35 |
|  | 68 | 47/20 | 68/20 | 47/20 | 120/35 | 120/35 | 120/35 |
|  | 100 | 47/20 | 68/20 | 47/20 | 120/35 | 120/35 | 120/35 |
|  | 150 | 47/20 | 68/20 | 47/20 | 120/35 | 120/35 | 120/35 |
|  | 220 | 47/20 | 68/20 | 47/20 | 120/35 | 120/35 | 120/35 |

### 9.2.1.2.3 Catch Diode Selection (D1)

In normal operation, the average current of the catch diode is the load current times the catch diode duty cycle, $1-\mathrm{D}$ ( D is the switch duty cycle, which is approximately the output voltage divided by the input voltage). The largest value of the catch diode average current occurs at the maximum load current and maximum input voltage (minimum D). For normal operation, the catch diode current rating must be at least 1.3 times greater than its maximum average current. However, if the power supply design must withstand a continuous output short, the diode must have a current rating equal to the maximum current limit of the LM2675. The most stressful condition for this diode is a shorted output condition (see Table 4). In this example, a $1-\mathrm{A}, 20-\mathrm{V}$ Schottky diode provides the best performance. If the circuit must withstand a continuous shorted output, TI recommends a Schottky diode of higher current.

The reverse voltage rating of the diode must be at least 1.25 times the maximum input voltage. Because of their fast switching speed and low forward voltage drop, Schottky diodes provide the best performance and efficiency. This Schottky diode must be located close to the LM2675 using short leads and short printed circuit traces.

Table 4. Schottky Diode Selection Table

| $\mathbf{V}_{\mathbf{R}}$ | 1-A DIODES |  | 3-A DIODES |  |
| :---: | :---: | :---: | :---: | :---: |
|  | SURFACE MOUNT | THROUGH HOLE | SURFACE MOUNT | THROUGH HOLE |
| 20 V | SK12 | 1N5817 | SK32 | 1N5820 |
|  | B120 | SR102 | - | SR302 |
| 30 V | SK13 | 1N5818 | SK33 | 1N5821 |
|  | B130 | 11DQ03 | 30WQ03F | 31DQ03 |
|  | MBRS130 | SR103 | - | - |
| 40 V | SK14 | 1N5819 | SK34 | 1N5822 |
|  | B140 | 11DQ04 | 30BQ040 | MBR340 |
|  | MBRS140 | SR104 | 30WQ04F | 31 DQ04 |
|  | 10BQ040 | - | MBRS340 | SR304 |
|  | 10MQ040 | - | MBRD340 | - |
|  | 15MQ040 | - | - | - |
| 50 V | SK15 | MBR150 | SK35 | MBR350 |
|  | B150 | 11DQ05 | 30WQ05F | $31 \mathrm{DQ05}$ |
|  | 10BQ050 | SR105 | - | SR305 |

### 9.2.1.2.4 Input Capacitor ( $\mathrm{C}_{\mathrm{IN}}$ )

A low ESR aluminum or tantalum bypass capacitor is needed between the input pin and ground to prevent large voltage transients from appearing at the input. This capacitor must be located close to the IC using short leads. In addition, the RMS current rating of the input capacitor must be selected to be at least $1 / 2$ the DC load current. The capacitor manufacturer data sheet must be checked to assure that this current rating is not exceeded. Figure 20 shows typical RMS current ratings for several different aluminum electrolytic capacitor values. A parallel connection of two or more capacitors may be required to increase the total minimum RMS current rating to suit the application requirements.


Figure 20. RMS Current Ratings for Low ESR Electrolytic Capacitors (Typical)

For an aluminum electrolytic capacitor, the voltage rating must be at least 1.25 times the maximum input voltage. Caution must be exercised if solid tantalum capacitors are used. The tantalum capacitor voltage rating must be twice the maximum input voltage. Table 3 shows the recommended application voltage for AVX TPS and Sprague 594D tantalum capacitors. TI also recommends that they be surge current tested by the manufacturer. The TPS series available from AVX, and the 593D and 594D series from Sprague are all surge current tested. Another approach to minimize the surge current stresses on the input capacitor is to add a small inductor in series with the input supply line.
Use caution when using ceramic capacitors for input bypassing, because it may cause severe ringing at the $\mathrm{V}_{\text {IN }}$ pin.
The important parameters for the input capacitor are the input voltage rating and the RMS current rating. With a maximum input voltage of 12 V , an aluminum electrolytic capacitor with a voltage rating greater than 15 V $\left(1.25 \times \mathrm{V}_{\mathrm{IN}}\right)$ would be needed. The next higher capacitor voltage rating is 16 V .

The RMS current rating requirement for the input capacitor in a buck regulator is approximately $1 / 2$ the DC load current. In this example, with a 1-A load, a capacitor with a RMS current rating of at least 500 mA is needed. The curves shown in Figure 20 can be used to select an appropriate input capacitor. From the curves, locate the 16-V line and note which capacitor values have RMS current ratings greater than 500 mA .

For a through hole design, a $330-\mu \mathrm{F}, 16-\mathrm{V}$ electrolytic capacitor (Panasonic HFQ series, Nichicon PL, Sanyo MVGX series or equivalent) would be adequate. Other types or other manufacturers' capacitors can be used provided the RMS ripple current ratings are adequate. Additionally, for a complete surface mount design, electrolytic capacitors such as the Sanyo CV-C or CV-BS and the Nichicon WF or UR and the NIC Components NACZ series could be considered.

For surface-mount designs, solid tantalum capacitors can be used, but caution must be exercised with regard to the capacitor surge current rating and voltage rating. In this example, checking Table 5, and the Sprague 594D series data sheet, a Sprague 594D $15-\mu \mathrm{F}, 25-\mathrm{V}$ capacitor is adequate.

Table 5. Sprague 594D

| RECOMMENDED APPLICATION VOLTAGE | VOLTAGE RATING |
| :---: | :---: |
| $\mathbf{8 5}^{\circ} \mathbf{C}$ RATING |  |
| 2.5 | 4 |
| 3.3 | 6.3 |
| 5 | 10 |
| 8 | 16 |
| 12 | 20 |
| 18 | 25 |
| 24 | 35 |
| 29 | 50 |

### 9.2.1.2.5 Boost Capacitor ( $\mathrm{C}_{\mathrm{B}}$ )

This capacitor develops the necessary voltage to turn the switch gate on fully. All applications must use a $0.01-\mu \mathrm{F}, 50-\mathrm{V}$ ceramic capacitor.

### 9.2.1.3 Application Curves



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### 9.2.2 Adjustable Output Voltage Application



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$\mathrm{C}_{\mathrm{IN}}=22-\mu \mathrm{F}, 50-\mathrm{V}$ Tantalum, Sprague 199D Series
Cout $=47-\mu \mathrm{F}, 25-\mathrm{V}$ Tantalum, Sprague 595D Series
D1 = 3.3-A, 50-V Schottky Rectifier, IR 30WQ05F
L1 $=68-\mu \mathrm{H}$ Sumida \#RCR110D-680L
R1 $=1.5 \mathrm{k} \Omega, 1 \%$
$C_{B}=0.01-\mu F, 50-\mathrm{V}$ Ceramic
Figure 24. Adjustable Output Voltage Schematic

### 9.2.2.1 Design Requirements

Table 1 lists the design requirements for the adjustable output voltage application.
Table 6. Design Parameters

| PARAMETER | VALUE |
| :---: | :---: |
| Regulated output voltage, $\mathrm{V}_{\text {OUT }}$ | 20 V |
| Maximum input voltage, $\mathrm{V}_{\text {IN }}(\max )$ | 28 V |
| Maximum load current, $\mathrm{I}_{\text {LOAD }}(\max )$ | 1 A |
| Switching frequency, F | Fixed at a nominal 260 kHz |

### 9.2.2.2 Detailed Design Procedure

### 9.2.2.2.1 Programming Output Voltage

Selecting $\mathrm{R}_{1}$ and $\mathrm{R}_{2}$, as shown in Figure 19.
Use Equation 1 to select the appropriate resistor values.
$V_{\text {OUT }}=V_{\text {REF }}\left(1+\frac{R_{2}}{R_{1}}\right)$
where

$$
\begin{equation*}
\text { - } \mathrm{V}_{\text {REF }}=1.21 \mathrm{~V} \tag{1}
\end{equation*}
$$

Select $R_{1}$ to be $1 \mathrm{k} \Omega, 1 \%$. Solve for $\mathrm{R}_{2}$ using Equation 2.

$$
\begin{equation*}
\mathrm{R}_{2}=\mathrm{R}_{1}\left(\frac{\mathrm{~V}_{\mathrm{OUT}}}{\mathrm{~V}_{\mathrm{REF}}}-1\right)=1 \mathrm{k} \Omega\left(\frac{20 \mathrm{~V}}{1.23 \mathrm{~V}}-1\right) \tag{2}
\end{equation*}
$$

Select a value for $\mathrm{R}_{1}$ between $240 \Omega$ and $1.5 \mathrm{k} \Omega$. The lower resistor values minimize noise pickup in the sensitive feedback pin. For the lowest temperature coefficient and the best stability with time, use $1 \%$ metal film resistors with Equation 3.

$$
\begin{equation*}
\mathrm{R}_{2}=\mathrm{R}_{1}\left(\frac{\mathrm{~V}_{\mathrm{OUT}}}{\mathrm{~V}_{\mathrm{REF}}}-1\right) \tag{3}
\end{equation*}
$$

$\mathrm{R}_{2}=1 \mathrm{k}(16.53-1)=15.53 \mathrm{k} \Omega$, closest $1 \%$ value is $15.4 \mathrm{k} \Omega$.
$R_{2}=15.4 \mathrm{k} \Omega$.

### 9.2.2.2.2 Inductor Selection (L1)

Calculate the inductor Volt $\times$ microsecond constant $\mathrm{E} \times \mathrm{T}(\mathrm{V} \times \mu \mathrm{s})$ from Equation 4.

$$
E \times T=\left(V_{I N(M A X)}-V_{O U T}-V_{S A T}\right) \times \frac{V_{O U T}+V_{D}}{V_{\text {IN(MAX })}-V_{S A T}+V_{D}} \times \frac{1000}{260}(V \times \mu \mathrm{S})
$$

where

- $\mathrm{V}_{\text {SAT }}=$ internal switch saturation voltage $=0.25 \mathrm{~V}$
- $\mathrm{V}_{\mathrm{D}}=$ diode forward voltage drop $=0.5 \mathrm{~V}$

Calculate the inductor Volt $\times$ microsecond constant $(E \times T)$ with Equation 5 .

$$
\begin{align*}
& E \times T=(28-20-0.25) \times \frac{20+0.5}{28-0.25+0.5} \times \frac{1000}{260}(\mathrm{~V} \times \mu \mathrm{s}) \\
& E \times T=(7.75) \times \frac{20.5}{28.25} \times 3.85(\mathrm{~V} \times \mu \mathrm{s}) \tag{5}
\end{align*}
$$

Use the $\mathrm{E} \times \mathrm{T}$ value from the previous formula and match it with the $\mathrm{E} \times \mathrm{T}$ number on the vertical axis of the inductor value selection guide in Figure 25. $\mathrm{E} \times \mathrm{T}=21.6(\mathrm{~V} \times \mu \mathrm{s})$.
On the horizontal axis, select the maximum load current (lioad $(\max )=1 \mathrm{~A})$.
Identify the inductance region intersected by the $\mathrm{E} \times \mathrm{T}$ value and the maximum load current value. Each region is identified by an inductance value and an inductor code (LXX). From the inductor value selection guide shown in Figure 25 , the inductance region intersected by the $21.6(\mathrm{~V} \times \mu \mathrm{s})$ horizontal line and the 1-A vertical line is $68 \mu \mathrm{H}$, and the inductor code is L30.
Select an appropriate inductor from the four manufacturer's part numbers listed in Table 2. For information on the different types of inductors, see the inductor selection in the fixed output voltage design procedure. From Table 2, locate line L30, and select an inductor part number from the list of manufacturers' part numbers.

### 9.2.2.2.3 Output Capacitor Selection ( $\mathrm{C}_{\text {out }}$ )

Select an output capacitor from the capacitor code selection guide in Table 7. Using the inductance value found in the inductor selection guide, step 1, locate the appropriate capacitor code corresponding to the desired output voltage. Use the appropriate row of the capacitor code selection guide, in Table 7. For this example, use the 15 V to 20 V row. The capacitor code corresponding to an inductance of $68 \mu \mathrm{H}$ is C20.

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Table 7. Capacitor Code Selection Guide

| $\begin{aligned} & \text { CTYLE }^{(1)} \end{aligned}$ | OUTPUT VOLTAGE (V) | INDUCTANCE ( $\mu \mathrm{H}$ ) |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  | 22 | 33 | 47 | 68 | 100 | 150 | 220 |
| SM and TH | 1.21 to 2.5 | - | - | - | - | C1 | C2 | C3 |
| SM and TH | 2.5 to 3.75 | - | - | - | C1 | C2 | C3 | C3 |
| SM and TH | 3.75 to 5 | - | - | C4 | C5 | C6 | C6 | C6 |
| SM and TH | 5 to 6.25 | - | C4 | C7 | C6 | C6 | C6 | C6 |
| SM and TH | 6.25 to 7.5 | C8 | C4 | C7 | C6 | C6 | C6 | C6 |
| SM and TH | 7.5 to 10 | C9 | C10 | C11 | C12 | C13 | C13 | C13 |
| SM and TH | 10 to 12.5 | C14 | C11 | C12 | C12 | C13 | C13 | C13 |
| SM and TH | 12.5 to 15 | C15 | C16 | C17 | C17 | C17 | C17 | C17 |
| SM and TH | 15 to 20 | C18 | C19 | C20 | C20 | C20 | C20 | C20 |
| SM and TH | 20 to 30 | C21 | C22 | C22 | C22 | C22 | C22 | C22 |
| TH | 30 to 37 | C23 | C24 | C24 | C25 | C25 | C25 | C25 |

(1) $\mathrm{SM}=$ surface mount, $\mathrm{TH}=$ through hole

Select an appropriate capacitor value and voltage rating, using the capacitor code, from the output capacitor selection table in Table 8. There are two solid tantalum (surface mount) capacitor manufacturers and four electrolytic (through hole) capacitor manufacturers to choose from. Tl recommends using both the manufacturers and the manufacturer's series that are listed in Table 8. From Table 8, choose a capacitor value (and voltage rating) that intersects the capacitor code(s) selected in section A, C20. The capacitance and voltage rating values corresponding to the capacitor code C20 are the surface mount and through hole.
Surface mount:

- $33-\mu \mathrm{F}, 25-\mathrm{V}$ Sprague 594D Series
- $33-\mu \mathrm{F}, 25-\mathrm{V}$ AVX TPS Series

Through hole:

- $33-\mu \mathrm{F}, 25-\mathrm{V}$ Sanyo OS-CON SC Series
- $120-\mu \mathrm{F}, 35-\mathrm{V}$ Sanyo MV-GX Series
- 120- $\mu \mathrm{F}, 35-\mathrm{V}$ Nichicon PL Series
- $120-\mu \mathrm{F}, 35-\mathrm{V}$ Panasonic HFQ Series

Other manufacturers or other types of capacitors may also be used, provided the capacitor specifications (especially the $100-\mathrm{kHz}$ ESR) closely match the characteristics of the capacitors listed in the output capacitor table. See the capacitor manufacturers' data sheet for this information.

Table 8. Output Capacitor Selection Table

| OUTPUT CAPACITOR |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| CAP. REF. DESG. \# | SURFACE MOUNT |  | THROUGH HOLE |  |  |  |
|  | $\begin{gathered} \text { SPRAGUE } \\ \text { 594D SERIES } \\ (\mu \mathrm{F} / \mathrm{V}) \\ \hline \end{gathered}$ | AVX TPS SERIES ( $\mu \mathrm{F} / \mathrm{V}$ ) | SANYO OS-CON SA SERIES ( $\mu \mathrm{F} / \mathrm{V}$ ) | $\begin{gathered} \text { SANYO MV-GX } \\ \text { SERIES } \\ (\mu \mathrm{F} / \mathrm{V}) \\ \hline \end{gathered}$ | NICHICON PL SERIES ( $\mu \mathrm{F} / \mathrm{V}$ ) | PANASONIC HFQ SERIES ( $\mu \mathrm{F} / \mathrm{V}$ ) |
| C1 | 120/6.3 | 100/10 | 100/10 | 220/35 | 220/35 | 220/35 |
| C2 | 120/6.3 | 100/10 | 100/10 | 150/35 | 150/35 | 150/35 |
| C3 | 120/6.3 | 100/10 | 100/35 | 120/35 | 120/35 | 120/35 |
| C4 | 68/10 | 100/10 | 68/10 | 220/35 | 220/35 | 220/35 |
| C5 | 100/16 | 100/10 | 100/10 | 150/35 | 150/35 | 150/35 |
| C6 | 100/16 | 100/10 | 100/10 | 120/35 | 120/35 | 120/35 |
| C7 | 68/10 | 100/10 | 68/10 | 150/35 | 150/35 | 150/35 |
| C8 | 100/16 | 100/10 | 100/10 | 330/35 | 330/35 | 330/35 |
| C9 | 100/16 | 100/16 | 100/16 | 330/35 | 330/35 | 330/35 |
| C10 | 100/16 | 100/16 | 68/16 | 220/35 | 220/35 | 220/35 |
| C11 | 100/16 | 100/16 | 68/16 | 150/35 | 150/35 | 150/35 |
| C12 | 100/16 | 100/16 | 68/16 | 120/35 | 120/35 | 120/35 |
| C13 | 100/16 | 100/16 | 100/16 | 120/35 | 120/35 | 120/35 |
| C14 | 100/16 | 100/16 | 100/16 | 220/35 | 220/35 | 220/35 |
| C15 | 47/20 | 68/20 | 47/20 | 220/35 | 220/35 | 220/35 |
| C16 | 47/20 | 68/20 | 47/20 | 150/35 | 150/35 | 150/35 |
| C17 | 47/20 | 68/20 | 47/20 | 120/35 | 120/35 | 120/35 |
| C18 | 68/25 | (2x) $33 / 25$ | 47/25 ${ }^{(1)}$ | 220/35 | 220/35 | 220/35 |
| C19 | 33/25 | 33/25 | $33 / 25^{(1)}$ | 150/35 | 150/35 | 150/35 |
| C20 | 33/25 | 33/25 | $33 / 25^{(1)}$ | 120/35 | 120/35 | 120/35 |
| C21 | 33/35 | (2x) 22/25 | See ${ }^{(2)}$ | 150/35 | 150/35 | 150/35 |
| C22 | 33/35 | 22/35 | $\mathrm{See}^{(2)}$ | 120/35 | 120/35 | 120/35 |
| C23 | See ${ }^{(2)}$ | See ${ }^{(2)}$ | See ${ }^{(2)}$ | 220/50 | 100/50 | 120/50 |
| C24 | $\mathrm{See}^{(2)}$ | $\mathrm{See}^{(2)}$ | $\mathrm{See}^{(2)}$ | 150/50 | 100/50 | 120/50 |
| C25 | See ${ }^{(2)}$ | See ${ }^{(2)}$ | See ${ }^{(2)}$ | 150/50 | 82/50 | 82/50 |

(1) The SC series of Os-Con capacitors (others are SA series)
(2) The voltage ratings of the surface mount tantalum chip and Os-Con capacitors are too low to work at these voltages.

### 9.2.2.2.4 Catch Diode Selection (D1)

In normal operation, the average current of the catch diode is the load current times the catch diode duty cycle, 1-D ( D is the switch duty cycle, which is approximately $\mathrm{V}_{\mathrm{OuT}} / \mathrm{V}_{\mathbb{I}}$ ). The largest value of the catch diode average current occurs at the maximum input voltage (minimum D). For normal operation, the catch diode current rating must be at least 1.3 times greater than its maximum average current. However, if the power supply design must withstand a continuous output short, the diode must have a current rating greater than the maximum current limit of the LM2675. The most stressful condition for this diode is a shorted output condition (see Table 4). Schottky diodes provide the best performance, and in this example a $1-\mathrm{A}, 40-\mathrm{V}$ Schottky diode would be a good choice. If the circuit must withstand a continuous shorted output, TI recommends a Schottky diode of higher current (at least 2.2 A ).
The reverse voltage rating of the diode must be at least 1.25 times the maximum input voltage. Because of their fast switching speed and low forward voltage drop, Schottky diodes provide the best performance and efficiency. The Schottky diode must be placed close to the LM2675 using short leads and short printed circuit traces.

### 9.2.2.2.5 Input Capacitor ( $\mathrm{C}_{\mathrm{IN}}$ )

A low ESR aluminum or tantalum bypass capacitor is needed between the input pin and ground to prevent large voltage transients from appearing at the input. This capacitor must be located close to the IC using short leads. In addition, the RMS current rating of the input capacitor must be selected to be at least $1 / 2$ the DC load current. The capacitor manufacturer data sheet must be checked to assure that this current rating is not exceeded. The curves shown in Figure 20 show typical RMS current ratings for several different aluminum electrolytic capacitor values. A parallel connection of two or more capacitors may be required to increase the total minimum RMS current rating to suit the application requirements.
For an aluminum electrolytic capacitor, the voltage rating must be at least 1.25 times the maximum input voltage. Caution must be exercised if solid tantalum capacitors are used. The tantalum capacitor voltage rating must be twice the maximum input voltage. Table 9 and Table 5 show the recommended application voltage for AVX TPS and Sprague 594D tantalum capacitors. TI recommends that they be surge current tested by the manufacturer. The TPS series available from AVX, and the 593D and 594D series from Sprague are all surge current tested. Another approach to minimize the surge current stresses on the input capacitor is to add a small inductor in series with the input supply line.

Table 9. AVX TPS

| RECOMMENDED APPLICATION VOLTAGE | VOLTAGE RATING |
| :---: | :---: |
| $\mathbf{8 5}^{\circ} \mathbf{C}$ RATING |  |
| 3.3 | 6.3 |
| 5 | 10 |
| 10 | 20 |
| 12 | 25 |
| 15 | 35 |

Use caution when using ceramic capacitors for input bypassing, because it may cause severe ringing at the $\mathrm{V}_{\mathbb{I N}}$ pin.
The important parameters for the input capacitor are the input voltage rating and the RMS current rating. With a maximum input voltage of 28 V , an aluminum electrolytic capacitor with a voltage rating of at least 35 V ( $1.25 \times$ $\mathrm{V}_{\mathrm{IN}}$ ) would be needed.
The RMS current rating requirement for the input capacitor in a buck regulator is approximately $1 / 2$ the DC load current. In this example, with a 1-A load, a capacitor with a RMS current rating of at least 500 mA is needed. The curves shown in Figure 20 can be used to select an appropriate input capacitor. From the curves, locate the $35-\mathrm{V}$ line and note which capacitor values have RMS current ratings greater than 500 mA .
For a through hole design, a $330-\mu F, 35-\mathrm{V}$ electrolytic capacitor (Panasonic HFQ series, Nichicon PL, Sanyo MVGX series or equivalent) would be adequate. Other types or other manufacturers' capacitors can be used provided the RMS ripple current ratings are adequate. Additionally, for a complete surface mount design, electrolytic capacitors such as the Sanyo CV-C or CV-BS, and the Nichicon WF or UR and the NIC Components NACZ series could be considered.
For surface mount designs, solid tantalum capacitors can be used, but caution must be exercised with regard to the capacitor surge current rating and voltage rating. In this example, checking Table 5, and the Sprague 594D series data sheet, a Sprague 594D $15-\mu \mathrm{F}, 50-\mathrm{V}$ capacitor is adequate.

### 9.2.2.2.6 Boost Capacitor ( $\mathrm{C}_{\mathrm{B}}$ )

This capacitor develops the necessary voltage to turn the switch gate on fully. All applications must use a $0.01-\mu \mathrm{F}, 50-\mathrm{V}$ ceramic capacitor.

### 9.2.2.3 Application Curve



Figure 25. LM2675, Adjustable Output

## 10 Power Supply Recommendations

The input voltage for the power supply is connected to the VIN pin. In addition to providing energy to the load the input voltage also provides bias for the internal circuitry of the LM2675. For ensured performance, the input voltage must be in the range of 6.5 V to 40 V . The VIN pin must always be bypassed with an input capacitor located close to this pin and GND.

LM2675
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## 11 Layout

### 11.1 Layout Guidelines

Layout is very important in switching regulator designs. Rapidly switching currents associated with wiring inductance can generate voltage transients which can cause problems. For minimal inductance and ground loops, the wires indicated by heavy lines (in Figure 19 and Figure 24) must be wide printed circuit traces and must be kept as short as possible. For best results, external components must be placed as close to the switcher IC as possible using ground plane construction or single-point grounding.
If open-core inductors are used, take special care as to the location and positioning of this type of inductor. Allowing the inductor flux to intersect sensitive feedback, IC ground path, and $\mathrm{C}_{\text {Out }}$ wiring can cause problems.
When using the adjustable version, take special care as to the location of the feedback resistors and the associated wiring. Physically locate both resistors near the IC, and route the wiring away from the inductor, especially an open-core type of inductor.

### 11.1.1 WSON Package Devices

The LM2675 is offered in the 16-pin WSON surface-mount package to allow for increased power dissipation compared to the SOIC and PDIP.
The die attach pad (DAP) can and must be connected to PCB Ground plane or island. For CAD and assembly guidelines see AN-1187 Leadless Leadframe Package (LLP).

### 11.2 Layout Examples



Figure 26. Typical Surface Mount PC Board Layout, Fixed Output

## Layout Examples (continued)


$\mathrm{C}_{\mathrm{IN}}=15-\mu \mathrm{F}, 50-\mathrm{V}$, Solid Tantalum Sprague 594D series
$\mathrm{C}_{\text {OUt }}=33-\mu \mathrm{F}$, 25-V, Solid Tantalum Sprague 594D series
D1 $=1-\mathrm{A}, 40-\mathrm{V}$ Schottky Rectifier, surface mount
L1 $=68-\mu \mathrm{H}$, L30, Coilcraft DO3316
$\mathrm{C}_{\mathrm{B}}=0.01-\mu \mathrm{F}, 50-\mathrm{V}$ ceramic
R1 $=1 \mathrm{k}, 1 \%$
R2 = Use formula in Detailed Design Procedure
Figure 27. Typical Surface Mount PC Board Layout, Adjustable Output

## 12 Device and Documentation Support

### 12.1 Documentation Support

### 12.1.1 Related Documentation

For related documentation see the following:

- AN-1187 Leadless Leadframe Package (LLP)
- LM2670 SIMPLE SWITCHER ${ }^{\circledR}$ High Efficiency 3A Step-Down Voltage Regulator with Sync


### 12.2 Receiving Notification of Documentation Updates

To receive notification of documentation updates, navigate to the device product folder on ti.com. In the upper right corner, click on Alert me to register and receive a weekly digest of any product information that has changed. For change details, review the revision history included in any revised document.

### 12.3 Community Resources

The following links connect to TI community resources. Linked contents are provided "AS IS" by the respective contributors. They do not constitute TI specifications and do not necessarily reflect TI's views; see TI's Terms of Use.
TI E2ETM Online Community TI's Engineer-to-Engineer (E2E) Community. Created to foster collaboration among engineers. At e2e.ti.com, you can ask questions, share knowledge, explore ideas and help solve problems with fellow engineers.
Design Support TI's Design Support Quickly find helpful E2E forums along with design support tools and contact information for technical support.

### 12.4 Trademarks

E2E is a trademark of Texas Instruments.
SIMPLE SWITCHER is a registered trademark of Texas Instruments.
All other trademarks are the property of their respective owners.

### 12.5 Electrostatic Discharge Caution

These devices have limited built-in ESD protection. The leads should be shorted together or the device placed in conductive foam during storage or handling to prevent electrostatic damage to the MOS gates.

### 12.6 Glossary

SLYZ022 - TI Glossary.
This glossary lists and explains terms, acronyms, and definitions.

## 13 Mechanical, Packaging, and Orderable Information

The following pages include mechanical, packaging, and orderable information. This information is the most current data available for the designated devices. This data is subject to change without notice and revision of this document. For browser-based versions of this data sheet, refer to the left-hand navigation.

TEXAS
PACKAGE OPTION ADDENDUM
INSTRUMENTS

## PACKAGING INFORMATION

| Orderable Device | Status <br> (1) | Package Type | Package Drawing | Pins | Package Qty | Eco Plan <br> (2) | Lead finish/ Ball material (6) | MSL Peak Temp <br> (3) | Op Temp ( ${ }^{\circ} \mathrm{C}$ ) | Device Marking <br> (4/5) | Samples |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| LM2675LD-5.0/NOPB | ACTIVE | WSON | NHN | 16 | 1000 | RoHS \& Green | SN | Level-3-260C-168 HR | -40 to 125 | S000FB | Samples |
| LM2675LD-ADJ/NOPB | ACTIVE | WSON | NHN | 16 | 1000 | RoHS \& Green | SN | Level-3-260C-168 HR | -40 to 125 | S000GB | Samples |
| LM2675M-12 | NRND | SOIC | D | 8 | 95 | Non-RoHS \& Green | Call TI | Level-1-235C-UNLIM | -40 to 125 | $\begin{aligned} & 2675 \\ & \mathrm{M}-12 \end{aligned}$ |  |
| LM2675M-12/NOPB | ACTIVE | SOIC | D | 8 | 95 | RoHS \& Green | NIPDAU \| SN | Level-1-260C-UNLIM | -40 to 125 | $\begin{aligned} & 2675 \\ & \mathrm{M}-12 \end{aligned}$ | Samples |
| LM2675M-3.3/NOPB | ACTIVE | SOIC | D | 8 | 95 | RoHS \& Green | NIPDAU \| SN | Level-1-260C-UNLIM | -40 to 125 | $\begin{array}{r} 2675 \\ \text { M3.3 } \\ \hline \end{array}$ | Samples |
| LM2675M-5.0 | NRND | SOIC | D | 8 | 95 | Non-RoHS \& Green | Call TI | Level-1-235C-UNLIM | -40 to 125 | $\begin{aligned} & 2675 \\ & \text { M5.0 } \end{aligned}$ |  |
| LM2675M-5.0/NOPB | ACTIVE | SOIC | D | 8 | 95 | RoHS \& Green | NIPDAU \| SN | Level-1-260C-UNLIM | -40 to 125 | $\begin{aligned} & 2675 \\ & \text { M5.0 } \\ & \hline \end{aligned}$ | Samples |
| LM2675M-ADJ | NRND | SOIC | D | 8 | 95 | Non-RoHS \& Green | Call TI | Level-1-235C-UNLIM | -40 to 125 | $\begin{aligned} & 2675 \\ & \text { MADJ } \end{aligned}$ |  |
| LM2675M-ADJ/NOPB | ACTIVE | SOIC | D | 8 | 95 | RoHS \& Green | NIPDAU \| SN | Level-1-260C-UNLIM | -40 to 125 | $\begin{aligned} & 2675 \\ & \text { MADJ } \\ & \hline \end{aligned}$ | Samples |
| LM2675MX-12/NOPB | ACTIVE | SOIC | D | 8 | 2500 | RoHS \& Green | NIPDAU \| SN | Level-1-260C-UNLIM | -40 to 125 | $\begin{aligned} & 2675 \\ & \mathrm{M}-12 \\ & \hline \end{aligned}$ | Samples |
| LM2675MX-3.3/NOPB | ACTIVE | SOIC | D | 8 | 2500 | RoHS \& Green | NIPDAU \| SN | Level-1-260C-UNLIM | -40 to 125 | $\begin{aligned} & 2675 \\ & \text { M3.3 } \end{aligned}$ | Samples |
| LM2675MX-5.0/NOPB | ACTIVE | SOIC | D | 8 | 2500 | RoHS \& Green | NIPDAU \| SN | Level-1-260C-UNLIM | -40 to 125 | $\begin{aligned} & 2675 \\ & \text { M5.0 } \end{aligned}$ | Samples |
| LM2675MX-ADJ/NOPB | ACTIVE | SOIC | D | 8 | 2500 | RoHS \& Green | NIPDAU \| SN | Level-1-260C-UNLIM | -40 to 125 | $\begin{aligned} & 2675 \\ & \text { MADJ } \end{aligned}$ | Samples |
| LM2675N-12/NOPB | ACTIVE | PDIP | P | 8 | 40 | RoHS \& Green | NIPDAU | Level-1-NA-UNLIM | -40 to 125 | LM2675 N-12 | Samples |
| LM2675N-3.3/NOPB | ACTIVE | PDIP | P | 8 | 40 | RoHS \& Green | NIPDAU | Level-1-NA-UNLIM | -40 to 125 | $\begin{aligned} & \hline \text { LM2675 } \\ & \text { N-3.3 } \\ & \hline \end{aligned}$ | Samples |
| LM2675N-5.0/NOPB | ACTIVE | PDIP | P | 8 | 40 | RoHS \& Green | NIPDAU | Level-1-NA-UNLIM | -40 to 125 | LM2675 N-5.0 | Samples |
| LM2675N-ADJ/NOPB | ACTIVE | PDIP | P | 8 | 40 | RoHS \& Green | NIPDAU | Level-1-NA-UNLIM | -40 to 125 | LM2675 N-ADJ | Samples |

${ }^{(1)}$ The marketing status values are defined as follows:
ACTIVE: Product device recommended for new designs.
LIFEBUY: TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.
NRND: Not recommended for new designs. Device is in production to support existing customers, but Tl does not recommend using this part in a new design.
PREVIEW: Device has been announced but is not in production. Samples may or may not be available.
OBSOLETE: TI has discontinued the production of the device.
${ }^{(2)}$ RoHS: TI defines "RoHS" to mean semiconductor products that are compliant with the current EU RoHS requirements for all 10 RoHS substances, including the requirement that RoHS substance do not exceed $0.1 \%$ by weight in homogeneous materials. Where designed to be soldered at high temperatures, "RoHS" products are suitable for use in specified lead-free processes. TI may reference these types of products as "Pb-Free"
RoHS Exempt: TI defines "RoHS Exempt" to mean products that contain lead but are compliant with EU RoHS pursuant to a specific EU RoHS exemption.
Green: TI defines "Green" to mean the content of Chlorine (Cl) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.
${ }^{(3)}$ MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.
${ }^{(4)}$ There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.
${ }^{(5)}$ Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a " $\sim$ " will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.
${ }^{(6)}$ Lead finish/Ball material - Orderable Devices may have multiple material finish options. Finish options are separated by a vertical ruled line. Lead finish/Ball material values may wrap to two lines if the finish value exceeds the maximum column width.

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NOTES:

1. Linear dimensions are in inches [millimeters]. Dimensions in parenthesis are for reference only. Controlling dimensions are in inches. Dimensioning and tolerancing per ASME Y14.5M.
2. This drawing is subject to change without notice.
3. This dimension does not include mold flash, protrusions, or gate burrs. Mold flash, protrusions, or gate burrs shall not exceed . 006 [0.15] per side.
4. This dimension does not include interlead flash.
5. Reference JEDEC registration MS-012, variation AA.


SOLDER MASK DETAILS

NOTES: (continued)
6. Publication IPC-7351 may have alternate designs.
7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.


NOTES: (continued)
8. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
9. Board assembly site may have different recommendations for stencil design.
$P(R-P D I P-T 8)$
PLASTIC DUAL-IN-LINE PACKAGE


NOTES: A. All linear dimensions are in inches (millimeters).
B. This drawing is subject to change without notice.
C. Falls within JEDEC MS-001 variation BA.


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    (2) Typical numbers are at $25^{\circ} \mathrm{C}$ and represent the most likely norm.

