





ZHCSF36A – DECEMBER 2015–REVISED MAY 2016

## LMR16010 SIMPLE SWITCHER<sup>®</sup> 60V、1A 降压转换器(Io 为 40µA)

Technical

Documents

Sample &

Buy

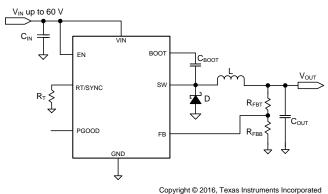
## 1 特性

- 输入电压范围: 4.3V 至 60V
- 1A 持续输出电流
- 40µA 超低工作静态电流
- 155mΩ 高侧金属氧化物半导体场效应晶体 (MOSFET)
- 电流模式控制
- 可调节开关频率范围: 200kHz 至 2.5MHz
- 与外部时钟频率同步
- 内部补偿方便使用
- 支持高占空比运行
- 精密使能引脚
- 电源正常状态标志
- 关断电流: 1µA
- 热保护、过压保护和短路保护
- 8 引脚 HSOIC PowerPAD™封装

## 2 应用范围

- 汽车电池稳压
- 工业用电源
- 电信和数据通信系统
- 通用宽 VIN 稳压

#### 简化电路原理图



## 3 说明

Tools &

Software

LMR16010 是一款集成高侧 MOSFET 的 60V、1A SIMPLE SWITCHER<sup>®</sup>降压稳压器。该器件具有 4.3V 至 60V 的宽输入电压范围,适用于从工业到汽车各类 应用 中非稳压电源的电源调节。该稳压器在休眠模式 下的静态电流为 40µA,非常适合电池供电类系统。并 且在关断模式下具有 1µA 的超低电流,可进一步延长 电池使用寿命。该稳压器的可调开关频率范围较宽,这 使得效率或外部元件尺寸能够得到优化。内部环路补偿 意味着用户不用承担设计环路补偿组件的枯燥工作。并 且还能够以最大限度减少器件的外部元件数。精密使能 输入简化了稳压器控制和系统电源排序。此外,该器件 还内置多种保护 特性: 逐周期电流限制保护、应对功 耗过大的热感测和热关断保护以及输出过压保护。

Support &

Community

**.**...

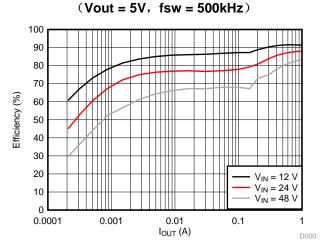
LMR16010 采用带有外露焊盘的 8 引脚 HSOIC 封装,用于实现低热阻。

#### 器件信息(1)

部件号	封装	封装尺寸(标称值)
LMR16010PDDAR	HSOIC (8)	4.89mm x 3.90mm

效率与输出电流间的关系

(1) 要了解所有可用封装,请见数据表末尾的可订购产品附录。



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NSTRUMENTS

EXAS

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## 4 修订历史记录

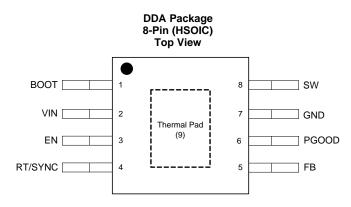
### Changes from Original (December 2015) to Revision A

已更改 完整版数据表中的"产品预览"至"量产数据"	. 1

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## 5 Pin Configuration and Functions



#### **Pin Functions**

PIN		<b>TYPE</b> <sup>(1)</sup>	DESCRIPTION	
NAME	NO.		DESCRIPTION	
BOOT	1	Р	Bootstrap capacitor connection for high-side MOSFET driver. Connect a high quality 0.1 $\mu\text{F}$ capacitor from BOOT to SW.	
VIN	2	Р	Connect to power supply and bypass capacitors $C_{IN}$ . Path from VIN pin to high frequency bypass $C_{IN}$ and GND must be as short as possible.	
EN	3	A	Enable pin, with internal pull-up current source. Pull below 1.2 V to disable. Float or conr to VIN to enable. Adjust the input under voltage lockout with two resistors. See the Enab and Adjusting Under voltage lockout section.	
RT/SYNC	4	A	Resistor Timing or External Clock input. An internal amplifier holds this pin at a fixed voltage when using an external resistor to ground to set the switching frequency. If the pin is pulled above the PLL upper threshold, a mode change occurs and the pin becomes a synchronization input. The internal amplifier is disabled and the pin is a high impedance clock input to the internal PLL. If clocking edges stop, the internal amplifier is re-enabled and the operating mode returns to frequency programming by resistor.	
FB	5	А	Feedback input pin, connect to the feedback divider to set $V_{\mbox{OUT}}.$ Do not short this pin to ground during operation.	
PGOOD	6	А	Power-Good pin, open drain output for power-good flag, use a 10 k $\Omega$ to 100 k $\Omega$ pull-up resistor to logic rail or other DC voltage no higher than 7 V.	
GND	7	G	System ground pin.	
SW	8	Р	Switching output of the regulator. Internally connected to high-side power MOSFET. Connect to power inductor.	
Thermal Pad	9	G	Major heat dissipation path of the die. Must be connected to ground plane on PCB.	

(1) A = Analog, P = Power, G = Ground

## 6 Specifications

### 6.1 Absolute Maximum Ratings

Over the recommended operating junction temperature range of -40 °C to 125 °C (unless otherwise noted) <sup>(1)</sup>

		MIN	MAX	UNIT
Input Voltages	VIN, EN to GND	-0.3	65	
	BOOT to GND	-0.3	71	
	FB to GND	-0.3	7	V
	RT/SYNC to GND	-0.3	3.6	
	PGOOD to GND	-0.3	7	
Output Voltages	BOOT to SW		6.5	V
	SW to GND	-3	65	V
TJ	Junction temperature	-40	150	°C
T <sub>stg</sub>	Storage temperature	-65	150	°C

(1) Stresses beyond those listed under Absolute Maximum Ratings may cause permanent damage to the device. These are stress ratings only, which do not imply functional operation of the device at these or any other conditions beyond those indicated under Recommended Operating Conditions. Exposure to absolute-maximum-rated conditions for extended periods may affect device reliability.

### 6.2 ESD Ratings

			VALUE	UNIT
	Flastrastatia disabarga	Human-body model (HBM) <sup>(1)</sup>	±2000	V
V(ESD)	V <sub>(ESD)</sub> Electrostatic discharge	Charged-device model (CDM) (2)	±500	v

(1) JEDEC document JEP155 states that 500-V HBM allows safe manufacturing with a standard ESD control process.

(2) JEDEC document JEP157 states that 250-V CDM allows safe manufacturing with a standard ESD control process.

## 6.3 Recommended Operating Conditions

Over the recommended operating junction temperature range of -40 °C to 125 °C (unless otherwise noted) <sup>(1)</sup>

		MIN	MAX	UNIT
Buck Regulator	VIN	4.3	60	
	VOUT	0.8	50	
	BOOT		66	V
	SW	-1	60	
	FB	0	5	
	EN	0	60	
Control	RT/SYNC	0	3.3	V
	PGOOD to GND	0	5	
Frequency	Switching frequency range at RT mode	200	2500	
Frequency	Switching frequency range at SYNC mode	250	2300	kHz
Temperature	Operating junction temperature, $T_J$	-40	125	°C

(1) Operating Ratings indicate conditions for which the device is intended to be functional, but do not guarantee specific performance limits. For guaranteed specifications, see *Electrical Characteristics*.

### 6.4 Thermal Information

		LMR16010	
	THERMAL METRIC <sup>(1)</sup> (2)	DDA (HSOIC)	UNIT
		8 PINS	
R <sub>θJA</sub>	Junction-to-ambient thermal resistance	42.5	°C/W
Ψ <sub>JT</sub>	Junction-to-top characterization parameter	9.9	°C/W
Ψ <sub>JB</sub>	Junction-to-board characterization parameter	25.4	°C/W
R <sub>0JC(top)</sub>	Junction-to-case (top) thermal resistance	56.1	°C/W
R <sub>0JC(bot)</sub>	Junction-to-case (bottom) thermal resistance	3.8	°C/W
$R_{\theta JB}$	Junction-to-board thermal resistance	25.5	°C/W

(1) For more information about traditional and new thermal metrics, see the Semiconductor and IC Package Thermal Metrics application report, SPRA953.

(2) Power rating at a specific ambient temperature T<sub>A</sub> should be determined with a maximum junction temperature (T<sub>J</sub>) of 125 °C, which is illustrated in *Recommended Operating Conditions* section.

### 6.5 Electrical Characteristics

Limits apply over the recommended operating junction temperature (T<sub>J</sub>) range of -40 °C to +125 °C, unless otherwise stated. Minimum and Maximum limits are specified through test, design or statistical correlation. Typical values represent the most likely parametric norm at  $T_J = 25$  °C, and are provided for reference purposes only. Unless otherwise specified, the following conditions apply:  $V_{IN} = 4.3$  V to 60 V

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
POWER SUP	PLY (VIN PIN)					
V <sub>IN</sub>	Operation input voltage		4.3		60	V
UVLO	Under voltage lockout thresholds	Rising threshold	3.8	4.0	4.2	V
		Hysteresis		285		mV
I <sub>SHDN</sub>	Shutdown supply current	$V_{EN} = 0 \text{ V}, \text{ T}_{A} = 25 \text{ °C}, 4.3 \text{ V} \le V_{IN} \le 60 \text{ V}$		1.0	3.0	μA
l <sub>Q</sub>	Operating quiescent current (non- switching)	V <sub>FB</sub> = 1.0 V, T <sub>A</sub> = 25 °C		40		μA
ENABLE (EN	PIN)	-				
V <sub>EN_TH</sub>	EN Threshold Voltage		1.05	1.20	1.38	V
I <sub>EN_PIN</sub>	EN PIN current	Enable threshold +50 mV		-4.6		
		Enable threshold -50 mV		-1.0		μA
I <sub>EN_HYS</sub>	EN hysteresis current			-3.6		μA
SOFT-STAR1	Г	-				
t <sub>SS</sub>	Internal soft-start time	10% to 90% of FB voltage		4.0		ms
POWER GOO	DD (PGOOD PIN)	· ·				
V <sub>PG_UV</sub>	Power-good flag under voltage tripping	POWER GOOD (% of FB voltage)		94		%
	threshold	POWER BAD (% of FB voltage)		92		%
V <sub>PG_OV</sub>	Power-good flag over voltage tripping	POWER BAD (% of FB voltage)		109		%
	threshold	POWER GOOD (% of FB voltage)		107		%
V <sub>PG_HYS</sub>	Power-good flag recovery hysteresis	% of FB voltage		2		%
I <sub>PG</sub>	PGOOD leakage current at high level output	V <sub>Pull-Up</sub> = 5 V		10	200	nA
V <sub>PG_LOW</sub>	PGOOD low level output voltage	I <sub>Pull-Up</sub> = 1 mA		0.1		V
V <sub>IN_PG_MIN</sub>	Minimum VIN for valid PGOOD output	$V_{Pull-Up} < 5 V \text{ at } I_{Pull-Up} = 100 \ \mu\text{A}$		1.6	1.95	V
VOLTAGE R	EFERENCE (FB PIN)	· · · ·				
V <sub>FB</sub>	Feedback voltage	T <sub>J</sub> = 25 °C	0.746	0.750	0.754	V
		T <sub>J</sub> = -40 °C to 125 °C	0.735	0.750	0.765	V

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## **Electrical Characteristics (continued)**

Limits apply over the recommended operating junction temperature (T<sub>J</sub>) range of -40 °C to +125 °C, unless otherwise stated. Minimum and Maximum limits are specified through test, design or statistical correlation. Typical values represent the most likely parametric norm at T<sub>J</sub> = 25 °C, and are provided for reference purposes only. Unless otherwise specified, the following conditions apply:  $V_{IN}$  = 4.3 V to 60 V

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
HIGH-SIDE MC	DSFET					
R <sub>DS_ON</sub>	On-resistance	$V_{IN}$ = 12 V, BOOT to SW = 5.8 V		155	320	mΩ
HIGH-SIDE MC	DSFET CURRENT LIMIT		·			
ILIMT	Current limit	V <sub>IN</sub> = 12 V, T <sub>A</sub> = 25 °C, Open Loop	1.45	1.75	2.1	Α
THERMAL PE	RFORMANCE					
T <sub>SHDN</sub>	Thermal shutdown threshold			170		- °C
T <sub>HYS</sub>	Hysteresis			12		



## 6.6 Switching Characteristics

Over the recommended operating junction temperature range of -40 °C to 125 °C (unless otherwise noted)

	PARAMETER	TEST CONDITIONS	MIN	TYP	MAX	UNIT
£	Switching frequency	$R_T = 11.5 \text{ k}\Omega$	1758	1912	2066	kHz
f <sub>SW</sub>	Switching frequency range at SYNC mode		250		2300	KIIZ
V <sub>SYNC_HI</sub>	SYNC clock high level threshold		1.7			v
V <sub>SYNC_LO</sub>	SYNC clock low level threshold				0.5	v
T <sub>SYNC_MIN</sub>	Minimum SYNC input pulse width	Measured at 500 kHz, $V_{SYNC_HI} > 3 V$ , $V_{SYNC_LO} < 0.3 V$		30		ns
T <sub>LOCK_IN</sub>	PLL lock in time	Measured at 500 kHz		100		μs
T <sub>ON_MIN</sub>	Minimum controllable on time	$V_{\text{IN}}$ = 12 V, BOOT to SW = 5.8 V, $I_{\text{Load}}$ = 1 A		90		ns
D <sub>MAX</sub>	Maximum duty cycle	f <sub>SW</sub> = 200 kHz		97%		

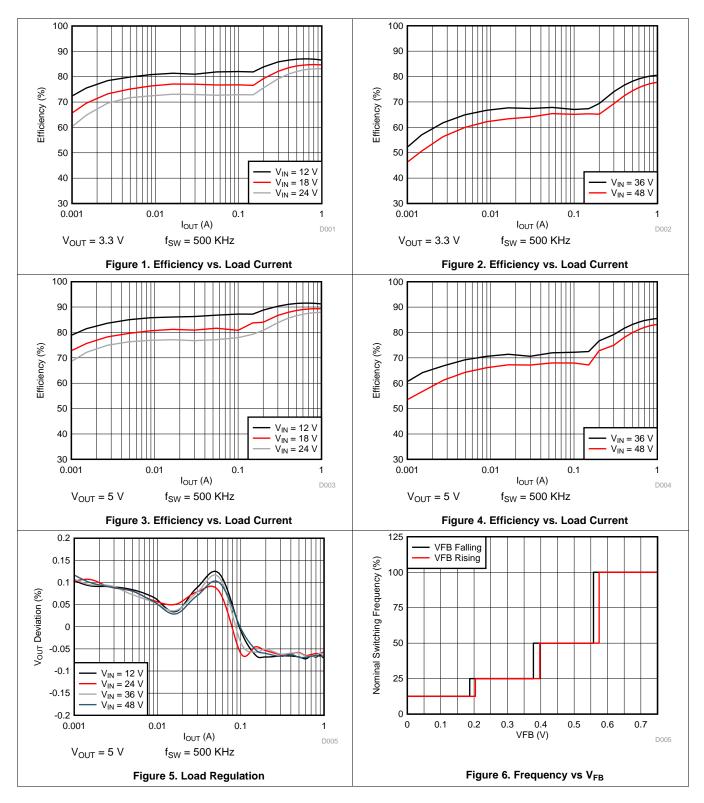
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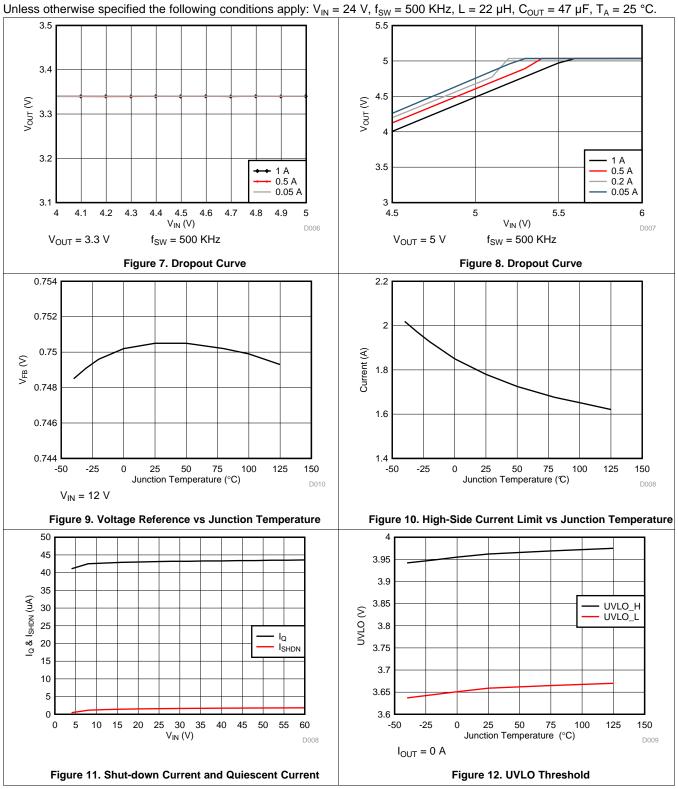
## 6.7 Typical Characteristics

Unless otherwise specified the following conditions apply:  $V_{IN}$  = 24 V,  $f_{SW}$  = 500 KHz, L = 22 µH,  $C_{OUT}$  = 47 µF,  $T_A$  = 25 °C.





### **Typical Characteristics (continued)**





## 7 Detailed Description

### 7.1 Overview

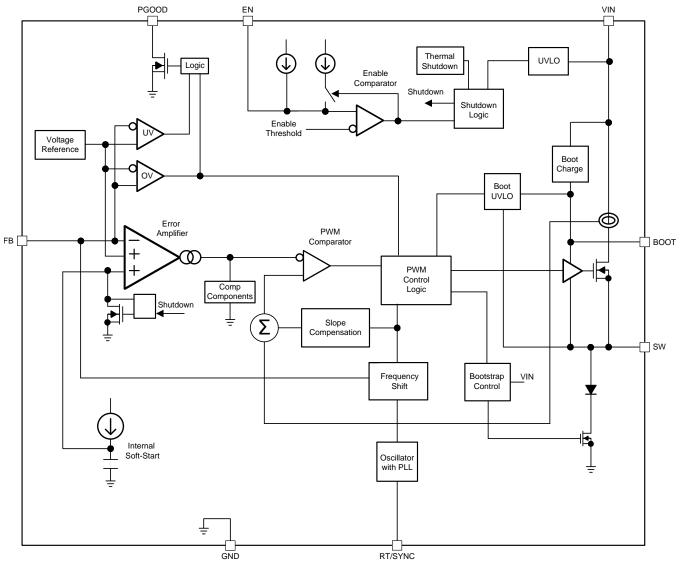
The LMR16010 SIMPLE SWITCHER<sup>®</sup> regulator is an easy to use step-down DC-DC converter that operates from a 4.3 V to 60 V supply voltage. It integrates a 155 m $\Omega$  (typical) high-side MOSFET, and is capable of delivering up to 1 A DC load current with exceptional efficiency and thermal performance in a very small solution size. The operating current is typically 40  $\mu$ A under no load condition (not switching). When the device is disabled, the supply current is typically 1  $\mu$ A. An extended family is available in 2 A and 3 A load options in pin to pin compatible packages.

The LMR16010 implements constant frequency peak current mode control with Sleep-mode at light load to achieve high efficiency. The device is internally compensated, which reduces design time, and requires fewer external components. The switching frequency is programmable from 200 kHz to 2.5 MHz by an external resistor  $R_T$ . The LMR16010 is also capable of synchronization to an external clock within the 250 kHz to 2.3 MHz frequency range, which allows the device to be optimized to fit small board space at higher frequency, or high efficient power conversion at lower frequency.

Other features are included for more comprehensive system requirements, including precision enable, and approximate 97% duty cycle by BOOT capacitor recharge circuit. These features provide a flexible and easy to use platform for a wide range of applications. Protection features include over temperature shutdown,  $V_{OUT}$  over voltage protection (OVP),  $V_{IN}$  under-voltage lockout (UVLO), cycle-by-cycle current limit, and short-circuit protection with frequency fold-back.



### 7.2 Functional Block Diagram



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## 7.3 Feature Description

#### 7.3.1 Fixed Frequency Peak Current Mode Control

The following operating description of the LMR16010 will refer to the *Functional Block Diagram* and to the waveforms in Figure 13. LMR16010 output voltage is regulated by turning on the high-side N-MOSFET with controlled ON time. During high-side switch ON time, the SW pin voltage swings up to approximately  $V_{IN}$ , and the inductor current  $i_L$  increase with linear slope  $(V_{IN} - V_{OUT}) / L$ . When high-side switch is off, inductor current discharges through freewheel diode with a slope of  $-V_{OUT} / L$ . The control parameter of Buck converter is defined as Duty Cycle D =  $t_{ON} / T_{SW}$ , where  $t_{ON}$  is the high-side switch ON time and  $T_{SW}$  is the switching period. The regulator control loop maintains a constant output voltage by adjusting the duty cycle D. In an ideal Buck converter, where losses are ignored, D is proportional to the output voltage and inversely proportional to the input voltage: D =  $V_{OUT} / V_{IN}$ .



### Feature Description (continued)

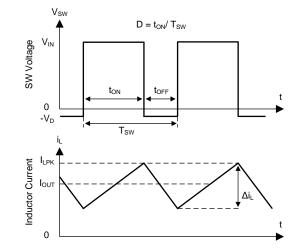


Figure 13. SW Node and Inductor Current Waveforms in Continuous Conduction Mode (CCM)

The LMR16010 employs fixed frequency peak current mode control. A voltage feedback loop is used to get accurate DC voltage regulation by adjusting the peak current command based on voltage offset. The peak inductor current is sensed from the high-side switch and compared to the peak current to control the ON time of the high-side switch. The voltage feedback loop is internally compensated, which allows for fewer external components, makes it easy to design, and provides stable operation with almost any combination of output capacitors. The regulator operates with fixed switching frequency at normal load condition. At very light load, the LMR16010 will operate in Sleep-mode to maintain high efficiency and the switching frequency will decrease with reduced load current.

#### 7.3.2 Slope Compensation

The LMR16010 adds a compensating ramp to the MOSFET switch current sense signal. This slope compensation prevents sub-harmonic oscillations at duty cycles greater than 50%. The peak current limit of the high-side switch is not affected by the slope compensation and remains constant over the full duty cycle range.

#### 7.3.3 Sleep-mode

The LMR16010 operates in Sleep-mode at light load currents to improve efficiency by reducing switching and gate drive losses. If the output voltage is within regulation and the peak switch current at the end of any switching cycle is below the current threshold of 300 mA, the device enters Sleep-mode. The Sleep-mode current threshold is the peak switch current level corresponding to a nominal internal COMP voltage of 400 mV.

When in Sleep-mode, the internal COMP voltage is clamped at 400 mV and the high-side MOSFET is inhibited, and the device draws only 40 µA (typical) input quiescent current. Since the device is not switching, the output voltage begins to decay. The voltage control loop responds to the falling output voltage by increasing the internal COMP voltage. The high-side MOSFET is enabled and switching resumes when the error amplifier lifts internal COMP voltage above 400 mV. The output voltage recovers to the regulated value, and internal COMP voltage eventually falls below the Sleep-mode threshold at which time the device again enters Sleep-mode.

#### 7.3.4 Low Dropout Operation and Bootstrap Voltage (BOOT)

The LMR16010 provides an integrated bootstrap voltage regulator. A small capacitor between the BOOT and SW pins provides the gate drive voltage for the high-side MOSFET. The BOOT capacitor is refreshed when the high-side MOSFET is off and the external low side diode conducts. The recommended value of the BOOT capacitor is 0.1  $\mu$ F. A ceramic capacitor with an X7R or X5R grade dielectric with a voltage rating of 16 V or greater is recommended for stable performance over temperature and voltage.



#### Feature Description (continued)

When operating with a low voltage difference from input to output, the high-side MOSFET of the LMR16010 will operate at approximate 97% duty cycle. When the high-side MOSFET is continuously on for 5 or 6 switching cycles (5 or 6 switching cycles for frequency lower than 1 MHz, and 10 or 11 switching cycles for frequency higher than 1 MHz) and the voltage from BOOT to SW drops below 3.2 V, the high-side MOSFET is turned off and an integrated low side MOSFET pulls SW low to recharge the BOOT capacitor.

Since the gate drive current sourced from the BOOT capacitor is small, the high-side MOSFET can remain on for many switching cycles before the MOSFET is turned off to refresh the capacitor. Thus the effective duty cycle of the switching regulator can be high, approaching 97%. The effective duty cycle of the converter during dropout is mainly influenced by the voltage drops across the power MOSFET, the inductor resistance, the low side diode voltage and the printed circuit board resistance.

#### 7.3.5 Adjustable Output Voltage

The internal voltage reference produces a precise 0.75 V (typical) voltage reference over the operating temperature range. The output voltage is set by a resistor divider from output voltage to the FB pin. It is recommended to use 1% tolerance or better and temperature coefficient of 100 ppm or less divider resistors. Select the low side resistor  $R_{FBB}$  for the desired divider current and use Equation 1 to calculate high-side  $R_{FBT}$ . Larger value divider resistors are good for efficiency at light load. However, if the values are too high, the regulator will be more susceptible to noise and voltage errors from the FB input current may become noticeable.  $R_{FBB}$  in the range from 10 k $\Omega$  to 100 k $\Omega$  is recommended for most applications.

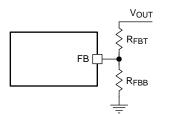


Figure 14. Output Voltage Setting

$$\mathsf{R}_{\mathsf{FBT}} = \frac{\mathsf{V}_{\mathsf{OUT}} - 0.75}{0.75} \times \mathsf{R}_{\mathsf{FBB}}$$

(1)

#### 7.3.6 Enable and Adjustable Under-voltage Lockout

The LMR16010 is enabled when the VIN pin voltage rises above 4.0 V (typical) and the EN pin voltage exceeds the enable threshold of 1.2 V (typical). The LMR16010 is disabled when the VIN pin voltage falls below 3.715 V (typical) or when the EN pin voltage is below 1.2 V (typical). The EN pin has an internal pull-up current source (typically  $I_{EN} = 1 \ \mu$ A) that enables operation of the LMR16010 when the EN pin is floating.

Many applications will benefit from the employment of an enable divider  $R_{ENT}$  and  $R_{ENB}$  in Figure 15 to establish a precision system UVLO level for the stage. System UVLO can be used for supplies operating from utility power as well as battery power. It can be used for sequencing, ensuring reliable operation, or supply protection, such as a battery. An external logic signal can also be used to drive EN input for system sequencing and protection.

When EN terminal voltage exceeds 1.2 V, an additional hysteresis current (typically  $I_{HYS} = 3.6 \ \mu$ A) is sourced out of EN terminal. When the EN terminal is pulled below 1.2 V,  $I_{HYS}$  current is removed. This additional current facilitates adjustable input voltage UVLO hysteresis. Use Equation 2 and Equation 3 to calculate  $R_{ENT}$  and  $R_{ENB}$  for desired UVLO hysteresis voltage.



(4)

#### Feature Description (continued)

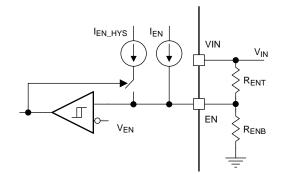


Figure 15. System UVLO By Enable Dividers

$$R_{ENT} = \frac{V_{START} - V_{STOP}}{I_{HYS}}$$

$$R_{ENB} = \frac{V_{EN}}{\frac{V_{START} - V_{EN}}{R_{ENT}} + I_{EN}}$$
(2)
(3)

where V<sub>START</sub> is the desired voltage threshold to enable LMR16010, V<sub>STOP</sub> is the desired voltage threshold to disable device,  $I_{EN} = 1 \ \mu A$  and  $I_{HYS} = 3.6 \ \mu A$  typically.

#### 7.3.7 Switching Frequency and Synchronization (RT/SYNC)

The switching frequency of the LMR16010 can be programmed by the resistor RT from the RT/SYNC pin and GND pin. The RT/SYNC pin can't be left floating or shorted to ground. To determine the timing resistance for a given switching frequency, use Equation 4 or the curve in Figure 16. Table 1 gives typical  $R_T$  values for a given  $f_{SW}$ .

$$R_{T}(k\Omega) = 42904 \times f_{SW}(kHz)^{-1.088}$$

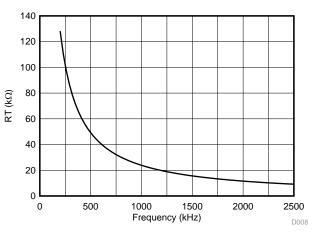


Figure 16. RT vs Frequency Curve

Table 1.	Typical	Frequency	Settina	RT	Resistance
			Journa		

f <sub>SW</sub> (kHz)	R <sub>T</sub> (kΩ)
200	133
350	73.2
500	49.9



#### **Feature Description (continued)**

f <sub>SW</sub> (kHz)	R <sub>T</sub> (kΩ)							
750	32.4							
1000	23.2							
1500	15.0							
1912	11.5							
2200	9.76							

Table 1. Typical Frequency Setting RT Resistance (continued)

The LMR16010 switching action can also be synchronized to an external clock from 250 kHz to 2.3 MHz. Connect a square wave to the RT/SYNC pin through either circuit network shown in Figure 17. Internal oscillator is synchronized by the falling edge of external clock. The recommendations for the external clock include: high level no lower than 1.7 V, low level no higher than 0.5 V and have a pulse width greater than 30 ns. When using a low impedance signal source, the frequency setting resistor  $R_T$  is connected in parallel with an AC coupling capacitor  $C_{COUP}$  to a termination resistor  $R_{TERM}$  (e.g., 50  $\Omega$ ). The two resistors in series provide the default frequency setting resistance when the signal source is turned off. A 10 pF ceramic capacitor can be used for  $C_{COUP}$ . Figure 18, Figure 19 and Figure 20 show the device synchronized to an external system clock.

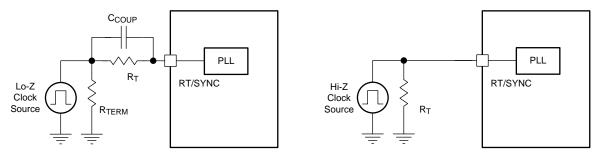
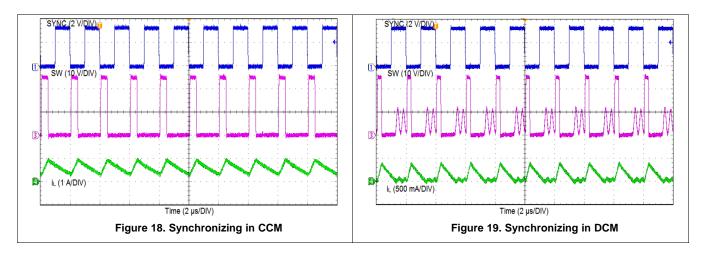


Figure 17. Synchronizing to an External Clock

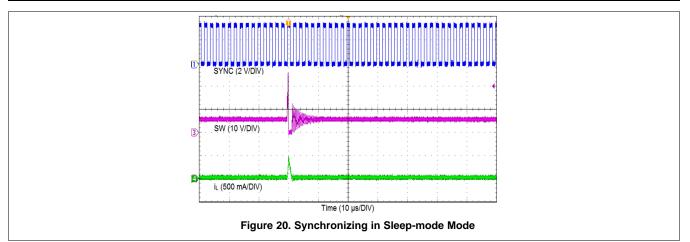


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Equation 5 calculates the maximum switching frequency limitation set by the minimum controllable on time and the input to output step down ratio. Setting the switching frequency above this value will cause the regulator to skip switching pulses to achieve the low duty cycle required at maximum input voltage.

$$f_{\text{SW(max)}} = \frac{1}{t_{\text{ON}}} \times \left( \frac{I_{\text{OUT}} \times R_{\text{IND}} + V_{\text{OUT}} + V_{\text{D}}}{V_{\text{IN}_{\text{MAX}}} - I_{\text{OUT}} \times R_{\text{DS}_{\text{ON}}} + V_{\text{D}}} \right)$$

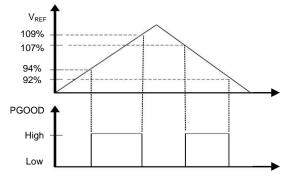
where

- I<sub>OUT</sub> = Output current
- R<sub>IND</sub> = Inductor series resistance
- V<sub>IN MAX</sub> = Maximum input voltage
- V<sub>OUT</sub> = Output voltage
- V<sub>D</sub> = Diode voltage drop
- R<sub>DS ON</sub> = High-side MOSFET switch on resistance
- $t_{ON} = Minimum on time$

#### 7.3.8 Power Good (PGOOD)

The LMR16010 has a built in power-good flag shown on PGOOD pin to indicate whether the output voltage is within its regulation level. The PGOOD signal can be used for start-up sequencing of multiple rails or fault protection. The PGOOD pin is an open-drain output that requires a pull-up resistor to an appropriate DC voltage. Voltage seen by the PGOOD pin should never exceed 7 V. A resistor divider pair can be used to divide the voltage down from a higher potential. A typical range of pull-up resistor value is 10 k $\Omega$  to 100 k $\Omega$ .

Refer to Figure 21. When the FB voltage is within the power-good band, +7% above and -6% below the internal reference  $V_{REF}$  typically, the PGOOD switch will be turned off and the PGOOD voltage will be pulled up to the voltage level defined by the pull-up resistor or divider. When the FB voltage is outside of the tolerance band, +9% above or -8% below  $V_{REF}$  typically, the PGOOD switch will be turned on and the PGOOD pin voltage will be pulled low to indicate power bad.





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(5)



#### 7.3.9 Over Current and Short Circuit Protection

The LMR16010 is protected from over current condition by cycle-by-cycle current limiting on the peak current of the high-side MOSFET. High-side MOSFET over-current protection is implemented by the nature of the Peak Current Mode control. The high-side switch current is compared to the output of the Error Amplifier (EA) minus slope compensation every switching cycle. Please refer to Functional Block Diagram for more details. The peak current of high-side switch is limited by a clamped maximum peak current threshold which is constant. So the peak current limit of the high-side switch is not affected by the slope compensation and remains constant over the full duty cycle range.

The LMR16010 also implements a frequency fold-back to protect the converter in severe over-current or short conditions. The oscillator frequency is divided by 2, 4, and 8 as the FB pin voltage decrease to 75%, 50%, 25% of  $V_{REF}$ . The frequency fold-back increases the off time by increasing the period of the switching cycle, so that it provides more time for the inductor current to ramp down and leads to a lower average inductor current. Lower frequency also means lower switching loss. Frequency fold-back reduces power dissipation and prevents overheating and potential damage to the device.

#### 7.3.10 Overvoltage Protection

The LMR16010 employs an output overvoltage protection (OVP) circuit to minimize voltage overshoot when recovering from output fault conditions or strong unload transients in designs with low output capacitance. The OVP feature minimizes output overshoot by turning off high-side switch immediately when FB voltage reaches to the rising OVP threshold which is nominally 109% of the internal voltage reference  $V_{REF}$ . When the FB voltage drops below the falling OVP threshold which is nominally 107% of  $V_{REF}$ , the high-side MOSFET resumes normal operation.

#### 7.3.11 Thermal Shutdown

The LMR16010 provides an internal thermal shutdown to protect the device when the junction temperature exceeds 170 °C (typical). The high-side MOSFET stops switching when thermal shundown activates. Once the die temperature falls below 158 °C (typical), the device reinitiates the power up sequence controlled by the internal soft-start circuitry.



#### 7.4 Device Functional Modes

#### 7.4.1 Shutdown Mode

The EN pin provides electrical ON and OFF control for the LMR16010. When  $V_{EN}$  is below 1.0 V, the device is in shutdown mode. The switching regulator is turned off and the quiescent current drops to 1.0  $\mu$ A typically. The LMR16010 also employs under voltage lock out protection. If  $V_{IN}$  voltage is below the UVLO level, the regulator will be turned off.

#### 7.4.2 Active Mode

The LMR16010 is in Active Mode when  $V_{EN}$  is above the precision enable threshold and  $V_{IN}$  is above its UVLO level. The simplest way to enable the LMR16010 is to connect the EN pin to VIN pin. This allows self startup when the input voltage is in the operation range: 4.3 V to 60 V. Please refer to *Enable and Adjustable Under-voltage Lockout* for details on setting these operating levels.

In Active Mode, depending on the load current, the LMR16010 will be in one of three modes:

- 1. Continuous conduction mode (CCM) with fixed switching frequency when load current is above half of the peak-to-peak inductor current ripple.
- 2. Discontinuous conduction mode (DCM) with fixed switching frequency when load current is lower than half of the peak-to-peak inductor current ripple in CCM operation.
- 3. Sleep-mode when internal COMP voltage drop to 400 mV at very light load.

#### 7.4.3 CCM Mode

CCM operation is employed in the LMR16010 when the load current is higher than half of the peak-to-peak inductor current. In CCM operation, the frequency of operation is fixed, output voltage ripple will be at a minimum in this mode and the maximum output current of 1 A can be supplied by the LMR16010.

#### 7.4.4 Light Load Operation

When the load current is lower than half of the peak-to-peak inductor current in CCM, the LMR16010 will operate in DCM. At even lighter current loads, Sleep-mode is activated to maintain high efficiency operation by reducing switching and gate drive losses.



### 8 Application and Implementation

#### NOTE

Information in the following applications sections is not part of the TI component specification, and TI does not warrant its accuracy or completeness. TI's customers are responsible for determining suitability of components for their purposes. Customers should validate and test their design implementation to confirm system functionality.

#### 8.1 Application Information

The LMR16010 is a step down DC-to-DC regulator. It is typically used to convert a higher DC voltage to a lower DC voltage with a maximum output current of 1 A. The following design procedure can be used to select components for the LMR16010. This section presents a simplified discussion of the design process.

#### 8.2 Typical Application

The LMR16010 only requires a few external components to convert from wide voltage range supply to a fixed output voltage. A schematic of 5 V / 1 A application circuit is shown in Figure 22. The external components have to fulfill the needs of the application, but also the stability criteria of the device's control loop.

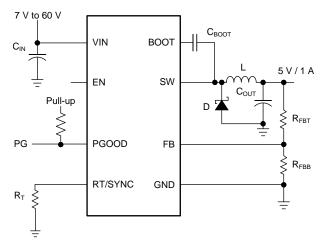


Figure 22. Application Circuit, 5V Output

#### 8.2.1 Design Requirements

This example details the design of a high frequency switching regulator using ceramic output capacitors. A few parameters must be known in order to start the design process. These parameters are typically determined at the system level:

Table 2	. Design	Parameters
---------	----------	------------

Input Voltage, V <sub>IN</sub>	7 V to 60 V, Typical 24 V				
Output Voltage, V <sub>OUT</sub>	5.0 V				
Maximum Output Current IO_MAX	1 A				
Transient Response 0.1 A to 1 A	5%				
Output Voltage Ripple	50 mV				
Input Voltage Ripple	400 mV				
Switching Frequency f <sub>SW</sub>	700 KHz				

#### 8.2.2 Detailed Design Procedure

#### 8.2.2.1 Output Voltage Set-Point

(7)

ISTRUMENTS

The output voltage of LMR16010 is externally adjustable using a resistor divider network. The divider network is comprised of top feedback resistor  $R_{FBT}$  and bottom feedback resistor  $R_{FBB}$ . Equation 6 is used to determine the output voltage:

$$\mathsf{R}_{\mathsf{FBT}} = \frac{\mathsf{V}_{\mathsf{OUT}} - 0.75}{0.75} \times \mathsf{R}_{\mathsf{FBB}} \tag{6}$$

Choose the value of  $R_{FBT}$  to be 100 k $\Omega$ . With the desired output voltage set to 5 V and the  $V_{FB} = 0.75$  V, the  $R_{FBB}$  value can then be calculated using Equation 6. The formula yields to a value 17.65 k $\Omega$ . Choose the closest available value of 17.8 k $\Omega$  for  $R_{FBB}$ .

#### 8.2.2.2 Switching Frequency

For desired frequency, use Equation 7 to calculate the required value for R<sub>T</sub>.

$$R_{T}(k\Omega) = 42904 \times f_{SW}(kHz)^{-1.088}$$

For 700 KHz, the calculated  $R_T$  is 34.44 k $\Omega$  and standard value 34.8 k $\Omega$  can be used to set the switching frequency at 700 KHz.

#### 8.2.2.3 Output Inductor Selection

The most critical parameters for the inductor are the inductance, saturation current and the RMS current. The inductance is based on the desired peak-to-peak ripple current  $\Delta i_L$ . Since the ripple current increases with the input voltage, the maximum input voltage is always used to calculate the minimum inductance  $L_{MIN}$ . Use Equation 8 to calculate the minimum value of the output inductor.  $K_{IND}$  is a coefficient that represents the amount of inductor ripple current relative to the maximum output current. A reasonable value of  $K_{IND}$  should be 20%-50% for 1 A output current. During an instantaneous short or over current operation event, the RMS and peak inductor current can be high. The inductor current rating should be higher than current limit.

$$\Delta i_{L} = \frac{V_{OUT} \times (V_{IN}MAX} - V_{OUT})}{V_{IN}MAX} \times L \times f_{SW}}$$

$$L_{MIN} = \frac{V_{IN}MAX} - V_{OUT}}{V_{IN}MAX} \times \frac{V_{OUT}}{V_{IN}MAX} - V_{OUT}}{V_{IN}MAX} \times \frac{V_{OUT}}{V_{IN}MAX} + V_{OUT}}{V_{IN}MAX} + V_{OUT}} \times \frac{V_{OUT}}{V_{IN}} + V_{OUT}}{V_{IN}} + V_{OUT} + V_{OUT}} \times \frac{V_{OUT}}{V_{IN}} + V_{OUT}} + V_{OUT} + V_{OU} + V_$$

 $= \frac{1}{I_{OUT} \times K_{IND}} \times \frac{V_{IN}_{MAX} \times f_{SW}}{V_{IN}_{MAX} \times f_{SW}}$ (9)

In general, it is preferable to choose lower inductance in switching power supplies, because it usually corresponds to faster transient response, smaller DCR, and reduced size for more compact designs. But too low of an inductance can generate too large of an inductor current ripple such that over current protection at the full load could be falsely triggered. It also generates more conduction loss since the RMS current is slightly higher. Larger inductor current ripple also implies larger output voltage ripple with same output capacitors. With peak current mode control, it is not recommended to have too small of an inductor current ripple. A larger peak current ripple improves the comparator signal to noise ratio.

For this design example, choose  $K_{IND} = 0.5$ , the minimum inductor value is calculated to be 13.1  $\mu$ H, and a nearest standard value is chosen: 12  $\mu$ H. A standard 12  $\mu$ H ferrite inductor with a capability of 1 A RMS current and 2 A saturation current can be used.

#### 8.2.2.4 Output Capacitor Selection

The output capacitor(s), C<sub>OUT</sub>, should be chosen with care since it directly affects the steady state output voltage ripple, loop stability and the voltage over/undershoot during load current transients.

The output ripple is essentially composed of two parts. One is caused by the inductor current ripple going through the Equivalent Series Resistance (ESR) of the output capacitors:

 $\Delta V_{OUT ESR} = \Delta i_L \times ESR = K_{IND} \times I_{OUT} \times ESR$ 

The other is caused by the inductor current ripple charging and discharging the output capacitors:

$$\Delta V_{OUT\_C} = \frac{\Delta i_{L}}{8 \times f_{SW} \times C_{OUT}} = \frac{K_{IND} \times I_{OUT}}{8 \times f_{SW} \times C_{OUT}}$$

. . . . . . .

(10)

(11)



The two components in the voltage ripple are not in phase, so the actual peak-to-peak ripple is smaller than the sum of two peaks.

Output capacitance is usually limited by transient performance specifications if the system requires tight voltage regulation with presence of large current steps and fast slew rate. When a fast large load increase happens, output capacitors provide the required charge before the inductor current can slew up to the appropriate level. The regulator's control loop usually needs three or more clock cycles to respond to the output voltage droop. The output capacitance must be large enough to supply the current difference for three clock cycles to maintain the output voltage within the specified range. Equation 12 shows the minimum output capacitors absorb energy stored in the inductor. The catch diode can't sink current so the energy stored in the inductor results in an output voltage overshoot. Equation 13 calculates the minimum capacitance required to keep the voltage overshoot within a specified range.

$$C_{OUT} > \frac{3 \times (I_{OH} - I_{OL})}{f_{SW} \times V_{US}}$$

$$C_{OUT} > \frac{I_{OH}^2 - I_{OL}^2}{(V_{OUT} + V_{OS})^2 - V_{OUT}^2} \times L$$
(12)
(13)

where

- $K_{IND}$  = Ripple ratio of the inductor ripple current ( $\Delta i_L / I_{OUT}$ )
- I<sub>OL</sub> = Low level output current during load transient
- I<sub>OH</sub> = High level output current during load transient
- V<sub>US</sub> = Target output voltage undershoot
- V<sub>OS</sub> = Target output voltage overshoot

For this design example, the target output ripple is 50 mV. Presuppose  $\Delta V_{OUT\_ESR} = \Delta V_{OUT\_C} = 50$  mV, and chose  $K_{IND} = 0.5$ . Equation 10 yields ESR no larger than 100 m $\Omega$  and Equation 11 yields  $C_{OUT}$  no smaller than 1.79  $\mu$ F. For the target over/undershoot range of this design,  $V_{US} = V_{OS} = 5\% \times V_{OUT} = 250$  mV. The  $C_{OUT}$  can be calculated to be no smaller than 15.4  $\mu$ F and 4.6  $\mu$ F by Equation 12 and Equation 13 respectively. In summary, the most stringent criteria for the output capacitor is 47  $\mu$ F. For this design example, one 47  $\mu$ F, 16 V, X7R ceramic capacitors with 5 m $\Omega$  ESR are used.

#### 8.2.2.5 Schottky Diode Selection

The breakdown voltage rating of the diode is preferred to be 25% higher than the maximum input voltage. The current rating for the diode should be equal to the maximum output current for best reliability in most applications. In cases where the input voltage is much greater than the output voltage the average diode current is lower. In this case it is possible to use a diode with a lower average current rating, approximately (1-D) ×  $I_{OUT}$  however the peak current rating should be higher than the maximum load current. A 1 A rated diode is a good starting point.

#### 8.2.2.6 Input Capacitor Selection

The LMR16010 device requires high frequency input decoupling capacitor(s) and a bulk input capacitor, depending on the application. The typical recommended value for the high frequency decoupling capacitor is 4.7  $\mu$ F to 10  $\mu$ F. A high-quality ceramic capacitor type X5R or X7R with sufficiency voltage rating is recommended. To compensate the derating of ceramic capacitors, a voltage rating of twice the maximum input voltage is recommended. Additionally, some bulk capacitance can be required, especially if the LMR16010 circuit is not located within approximately 5 cm from the input voltage source. This capacitor is used to provide damping to the voltage spike due to the lead inductance of the cable or the trace. For this design, two 2.2  $\mu$ F, X7R ceramic capacitors rated for 100 V are used. A 0.1  $\mu$ F for high-frequency filtering and place it as close as possible to the device pins.

#### 8.2.2.7 Bootstrap Capacitor Selection

Every LMR16010 design requires a bootstrap capacitor ( $C_{BOOT}$ ). The recommended capacitor is 0.1  $\mu$ F and rated 16 V or higher. The bootstrap capacitor is located between the SW pin and the BOOT pin. The bootstrap capacitor must be a high-quality ceramic type with an X7R or X5R grade dielectric for temperature stability.

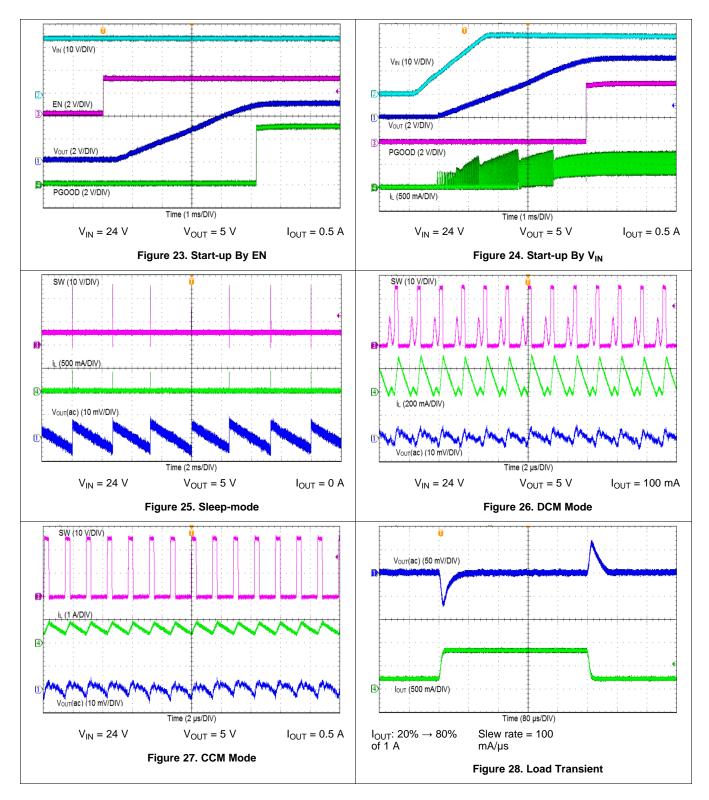
LMR16010

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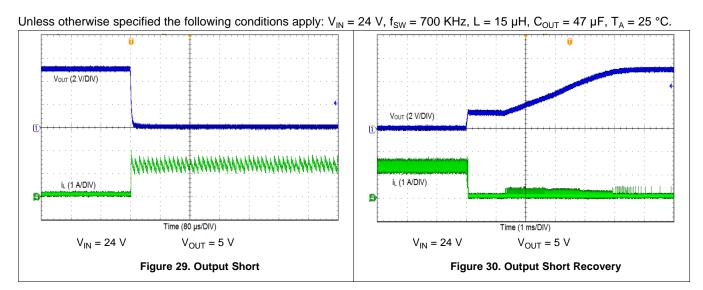
#### 8.2.3 Application Curves

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Unless otherwise specified the following conditions apply:  $V_{IN}$  = 24 V,  $f_{SW}$  = 700 KHz, L = 15 µH,  $C_{OUT}$  = 47 µF,  $T_A$  = 25 °C.







## 9 Power Supply Recommendations

The LMR16010 is designed to operate from an input voltage supply range between 4.3 V and 60 V. This input supply should be able to withstand the maximum input current and maintain a stable voltage. The resistance of the input supply rail should be low enough that an input current transient does not cause a high enough drop at the LMR16010 supply voltage that can cause a false UVLO fault triggering and system reset. If the input supply is located more than a few inches from the LMR16010, additional bulk capacitance may be required in addition to the ceramic input capacitors. The amount of bulk capacitance is not critical, but a 22  $\mu$ F or 47  $\mu$ F electrolytic capacitor is a typical choice .

## 10 Layout

### **10.1 Layout Guidelines**

Layout is a critical portion of good power supply design. The following guidelines will help users design a PCB with the best power conversion performance, thermal performance, and minimized generation of unwanted EMI.

- 1. The feedback network, resistor R<sub>FBT</sub> and R<sub>FBB</sub>, should be kept close to the FB pin. V<sub>OUT</sub> sense path away from noisy nodes and preferably through a layer on the other side of a shielding layer.
- 2. The input bypass capacitor C<sub>IN</sub> must be placed as close as possible to the VIN pin and ground. Grounding for both the input and output capacitors should consist of localized top side planes that connect to the GND pin and PAD.
- 3. The inductor L should be placed close to the SW pin to reduce magnetic and electrostatic noise.
- 4. The output capacitor, C<sub>OUT</sub> should be placed close to the junction of L and the diode D. The L, D, and C<sub>OUT</sub> trace should be as short as possible to reduce conducted and radiated noise and increase overall efficiency.
- 5. The ground connection for the diode,  $C_{IN}$ , and  $C_{OUT}$  should be as small as possible and tied to the system ground plane in only one spot (preferably at the  $C_{OUT}$  ground point) to minimize conducted noise in the system ground plane.
- 6. For more detail on switching power supply layout considerations see SNVA021 Application Note AN-1149.



## 10.2 Layout Example

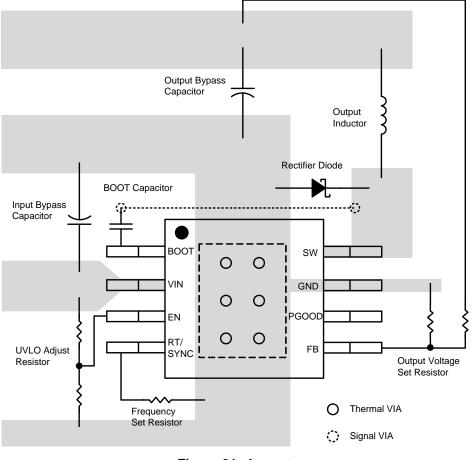


Figure 31. Layout

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## 11 器件和文档支持

### 11.1 器件支持

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#### 11.5 Glossary

#### SLYZ022 — TI Glossary.

This glossary lists and explains terms, acronyms, and definitions.



## 12 机械、封装和可订购信息

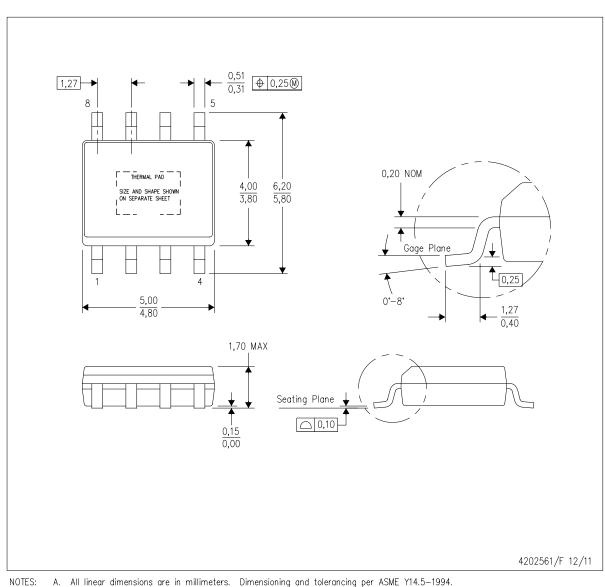
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## **MECHANICAL DATA**

PowerPAD<sup>™</sup> PLASTIC SMALL-OUTLINE



- - This drawing is subject to change without notice. Β.
  - C. Body dimensions do not include mold flash or protrusion not to exceed 0,15.
  - D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>.
  - E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions.
     F. This package complies to JEDEC MS-012 variation BA

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## PACKAGING INFORMATION

Orderable Device	Status (1)	Package Type	Package Drawing	Pins	Package Qty	Eco Plan (2)	Lead finish/ Ball material (6)	MSL Peak Temp (3)	Op Temp (°C)	Device Marking (4/5)	Samples
LMR16010PDDA	ACTIVE	SO PowerPAD	DDA	8	75	RoHS & Green	NIPDAU   NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	SB1P	Samples
LMR16010PDDAR	ACTIVE	SO PowerPAD	DDA	8	2500	RoHS & Green	NIPDAU   NIPDAUAG	Level-2-260C-1 YEAR	-40 to 125	SB1P	Samples

<sup>(1)</sup> The marketing status values are defined as follows:

ACTIVE: Product device recommended for new designs.

**LIFEBUY:** TI has announced that the device will be discontinued, and a lifetime-buy period is in effect.

NRND: Not recommended for new designs. Device is in production to support existing customers, but TI does not recommend using this part in a new design.

**PREVIEW**: Device has been announced but is not in production. Samples may or may not be available.

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Green: TI defines "Green" to mean the content of Chlorine (CI) and Bromine (Br) based flame retardants meet JS709B low halogen requirements of <=1000ppm threshold. Antimony trioxide based flame retardants must also meet the <=1000ppm threshold requirement.

<sup>(3)</sup> MSL, Peak Temp. - The Moisture Sensitivity Level rating according to the JEDEC industry standard classifications, and peak solder temperature.

<sup>(4)</sup> There may be additional marking, which relates to the logo, the lot trace code information, or the environmental category on the device.

<sup>(5)</sup> Multiple Device Markings will be inside parentheses. Only one Device Marking contained in parentheses and separated by a "~" will appear on a device. If a line is indented then it is a continuation of the previous line and the two combined represent the entire Device Marking for that device.

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## PACKAGE OPTION ADDENDUM

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## TUBE



## - B - Alignment groove width

\*All dimensions are nominal

Device	Package Name	Package Type	Pins	SPQ	L (mm)	W (mm)	Τ (μm)	B (mm)
LMR16010PDDA	DDA	HSOIC	8	75	517	7.87	635	4.25
LMR16010PDDA	DDA	HSOIC	8	75	507	8	3940	4.32

## **DDA0008B**



## **PACKAGE OUTLINE**

## PowerPAD<sup>™</sup> SOIC - 1.7 mm max height

PLASTIC SMALL OUTLINE



#### NOTES:

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- 4. This dimension does not include interlead flash. Interlead flash shall not exceed 0.25 mm per side.
- 5. Reference JEDEC registration MS-012.



## DDA0008B

## **EXAMPLE BOARD LAYOUT**

## PowerPAD<sup>™</sup> SOIC - 1.7 mm max height

PLASTIC SMALL OUTLINE



NOTES: (continued)

- 6. Publication IPC-7351 may have alternate designs.
- 7. Solder mask tolerances between and around signal pads can vary based on board fabrication site.
- This package is designed to be soldered to a thermal pad on the board. For more information, see Texas Instruments literature numbers SLMA002 (www.ti.com/lit/slma002) and SLMA004 (www.ti.com/lit/slma004).
- 9. Size of metal pad may vary due to creepage requirement.
- 10. Vias are optional depending on application, refer to device data sheet. If any vias are implemented, refer to their locations shown on this view. It is recommended that vias under paste be filled, plugged or tented.



## DDA0008B

## **EXAMPLE STENCIL DESIGN**

## PowerPAD<sup>™</sup> SOIC - 1.7 mm max height

PLASTIC SMALL OUTLINE



NOTES: (continued)

- 11. Laser cutting apertures with trapezoidal walls and rounded corners may offer better paste release. IPC-7525 may have alternate design recommendations.
- 12. Board assembly site may have different recommendations for stencil design.



PowerPAD ™ PLASTIC SMALL-OUTLINE



- B. This drawing is subject to change without notice.
- C. Body dimensions do not include mold flash or protrusion not to exceed 0,15.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 for information regarding recommended board layout. This document is available at www.ti.com <a href="http://www.ti.com">http://www.ti.com</a>.
- E. See the additional figure in the Product Data Sheet for details regarding the exposed thermal pad features and dimensions.
- F. This package complies to JEDEC MS-012 variation BA

PowerPAD is a trademark of Texas Instruments.



# PowerPAD<sup>™</sup> PLASTIC SMALL OUTLINE

## THERMAL INFORMATION

This PowerPAD<sup> $\mathbb{N}$ </sup> package incorporates an exposed thermal pad that is designed to be attached to a printed circuit board (PCB). The thermal pad must be soldered directly to the PCB. After soldering, the PCB can be used as a heatsink. In addition, through the use of thermal vias, the thermal pad can be attached directly to the appropriate copper plane shown in the electrical schematic for the device, or alternatively, can be attached to a special heatsink structure designed into the PCB. This design optimizes the heat transfer from the integrated circuit (IC).

For additional information on the PowerPAD package and how to take advantage of its heat dissipating abilities, refer to Technical Brief, PowerPAD Thermally Enhanced Package, Texas Instruments Literature No. SLMA002 and Application Brief, PowerPAD Made Easy, Texas Instruments Literature No. SLMA004. Both documents are available at www.ti.com.

The exposed thermal pad dimensions for this package are shown in the following illustration.



Exposed Thermal Pad Dimensions

4206322-6/L 05/12

NOTE: A. All linear dimensions are in millimeters

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PowerPAD<sup>™</sup> PLASTIC SMALL OUTLINE



NOTES: A. All linear dimensions are in millimeters.

- B. This drawing is subject to change without notice.
- C. Publication IPC-7351 is recommended for alternate designs.
- D. This package is designed to be soldered to a thermal pad on the board. Refer to Technical Brief, PowerPad Thermally Enhanced Package, Texas Instruments Literature No. SLMA002, SLMA004, and also the Product Data Sheets for specific thermal information, via requirements, and recommended board layout. These documents are available at www.ti.com <http://www.ti.com>. Publication IPC-7351 is recommended for alternate designs.
- E. Laser cutting apertures with trapezoidal walls and also rounding corners will offer better paste release. Customers should contact their board assembly site for stencil design recommendations. Example stencil design based on a 50% volumetric metal load solder paste. Refer to IPC-7525 for other stencil recommendations.
- F. Customers should contact their board fabrication site for solder mask tolerances between and around signal pads. PowerPAD is a trademark of Texas Instruments.



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